

## Mechanical Properties of Tetrafluoro skateboard rubber bearings under nitric and sulphuric acids Condition

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**Abstract.** The present study was conducted to obtain a better understanding of the variation rule of compressive mechanical properties of tetrafluoro skateboard rubber bearings under nitric and sulphuric acids Condition. A total of 5 specimens were processed in a nitric and sulphuric acids PH4.5, and one specimen was in natural state. The parameter mainly considered time of nitric and sulphuric acids aging processing for specimens. The compressive capacity, ultimate compressive strength and compressive elastic modulus of tetrafluoro skateboard rubber bearings decreased dramatically. The attenuation models conform to reality well which shows that this model is applicable and has vast prospect in assessing the performance of tetrafluoro skateboard rubber bearings under nitric and sulphuric acids condition.

### Introduction

In order to study the effect of nitrate sulphuric acid on the mechanical properties of the rubber bearing of the Teflon slide plate of the highway bridge[1-5]. A total of 5 specimens were processed in a nitric and sulphuric acids PH4.5 chamber. After that, five specimens were tested subjected to axial load. The failure modes and mechanical properties are presented and discussed, and the attenuation trends of ultimate compressive strength and compressive elastic modulus of laminated tetrafluoro skateboard rubber bearings under nitric and sulphuric acids aging condition are analyzed. Finally, the attenuation models of ultimate compressive strength and compressive elastic modulus laminated tetrafluoro skateboard rubber bearings are acquired by regressing data of experiment with the least square method.

### Experimental Program

The main goal of the experimental research was to obtain the variation rule of mechanical properties of tetrafluoro skateboard rubber bearings under nitric and sulphuric acids condition.

Fig. 1 shows modes of acid corrosion treatment of PTFE slide rubber bearings. Different grouping with sodium sulfate treatment of PTFE slide rubber bearings is described in Table 1.

All test specimens were made in Chinese Hengshui Xinli Engineering Inc.

A total of 5 specimens were tested. There were 0, 20, 40, 60 and 80 days nitric and sulphuric acids aging processing for specimens. The Dimensions of specimens have no obvious change after aging processing. Change with size of PTFE slide rubber bearings are described in Table 2.

The compression tests were carried out in the Structural Engineering Laboratory of Shenyang Jianzhu University. The compression load was applied by a 5000kN pressure testing machine.

The specimens were subjected to vertical load, and its loading regimes were described as follows:

(1) The centre of specimens should be adjusted geometrically and physically before preloading. The specimens were loaded to compressive stress 1.0MPa and displacement sensors were set up.

(2) The specimens were preloaded to permissible compressive stress [ $\sigma$ ] and keep invariable load 5 minutes. Then, the specimens were unloaded to compressive stress 1.0MPa.

(3) the tests of compressive elastic modulus: The specimens were increased 1.0MPa every time from compressive stress 1.0MPa after preloading three times and keep invariable load 3 minutes until the specimens were loaded to  $[S]$ . Then, the specimens were unloaded to compressive stress 1.0MPa. Loading repeated after 10 minutes, and the loading process continued 3 times.

(4) The tests of ultimate compressive strength: The specimens were increased 1.0MPa every one minute after the tests of compressive elastic modulus until the specimens were loaded to 7  $[S]$ .

Tab.1 Aging Processing of Specimens

NO	specimens	days of sulphuric acids aging processing
1	GJZF4200×300×43ZYBZ01	0
2	GJZF4200×300×43ZYXL020	20
3	GJZF4200×300×43ZYXL040	40
4	GJZF4200×300×43ZYXL060	60
5	GJZF4200×300×43ZYXL080	80
6	GJZF4200×300×43ZYXL100	100



Fig.1. Shape of a test specimen

Tab2.CHANGE WITH SIZE OF PTFE SLIDE RUBBER BEARINGS

loading modes	specimen	days of thermal aging processing	Dimensions before sulphuric acids aging processing (mm)	Dimensions after sulphuric acids aging processing (mm)
Compression test	GJZF4200×300×43ZYBZ01	0	200×301×41	—
	GJZF4200×300×43ZYXL020	20	202×301×41	202×301×43
	GJZF4200×300×43ZYXL040	40	200×300×41	199×301×41
	GJZF4200×300×43ZYXL060	60	201×301×42	200×301×43
	GJZF4200×300×43ZYXL080	80	199×301×43	199×300×42
	GJZF4200×300×43ZYXL100	100	200×300×41	201×299×41

## Experimental Results

Fig.2 shows failure modes of specimens in compression test. The vertical load increased gradually, specimens were in elastic state when the cracks did not appear. Loading were in a short stagnation when a few fine cracks appeared around agglutinate places of steel plates and rubber of specimens' edge. After that, the vertical displacement increased slowly, but the horizontal displacement increased sharply with load increasing. Meanwhile, protrusions appeared around specimens' edge, and the cracks got larger and deeper fast. The vertical displacement and horizontal displacement increased slowly and load declined precipitously when specimens devastated. The layer-crack damage characteristics of specimens were obvious because steel plates broke away from rubber. The specimens after thermal aging processing were more probably brittle failure than the standard specimen. Moreover, the exposure of steel plate, cracks and other failure phenomena were more serious than the standard specimen.

The mechanical properties of specimens are shown in table 3. The compressive capacity, ultimate compressive strength and compressive elastic modulus of the specimens decreased obviously with the increasing in time of d sulphuric acids aging processing.



Fig2. Failure modes of specimens

Tab3. COMPARISON OF DIFFERENT SODIUM SULFATE INDEX NUMBER OF PTFE SLIDE RUBBER BEARINGS

Specimen	Compressive capacity (kN)	Ultimate compressive strength (MPa)	Displacement corresponding to ultimate compressive strength (mm)			Displacement corresponding to compressive stress 70 MPa (mm)		
			vertical	horizontal longitudinal	horizontal lateral	vertical	horizontal longitudinal	horizontal lateral
GJZF4200×300×43ZYBZ01	4408.60	73.48	4.11	4.51	3.15	3.73	3.98	2.75
GJZF4200×300×43ZYXL020	4169.20	69.49	3.89	3.89	2.82	3.96	3.99	2.91
GJZF4200×300×43ZYXL040	4163.50	69.39	3.59	4.20	3.55	4.02	3.89	3.65
GJZF4200×300×43ZYXL060	4160.80	69.35	3.37	4.48	4.30	3.42	4.69	4.51
GJZF4200×300×43ZYXL080	4155.60	69.26	4.21	3.99	4.52	4.28	4.22	4.79
GJZF4200×300×43ZYXL100	4152.30	69.21	4.00	3.47	5.03	4.05	3.59	5.37

### Test Analysis

Fig.3 shows the attenuation curve of compressive capacity of tetrafluoro skateboard rubber bearings under nitric and sulphuric acids. The sulphuric acids aging processing has a significant impact on compressive capacity of 1 tetrafluoro skateboard rubber bearings. The compressive capacity decreased dramatically with the increasing in aging time.

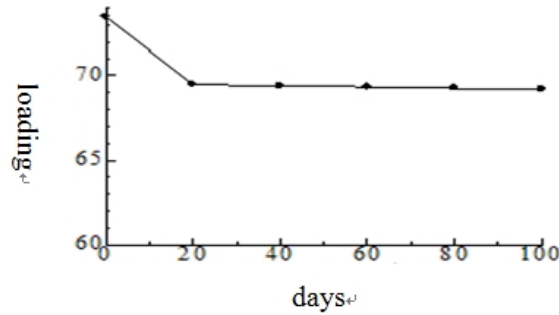


Fig 3. Attenuation curve of ultimate compressive strength

The attenuation model is acquired by regressing data of experiment with the least square method. Fig.4 shows the attenuation curve of ultimate compressive strength of laminated tetrafluoro skateboard rubber bearings. The attenuation function is shown as follows<sup>[6-11]</sup>:

$$y=69.547^{-0.001x} \quad (1)$$

Where, y is ultimate compressive strength; x is years of nitric and sulphuric acids aging.

The attenuation model of ultimate compressive strength conform to reality well which shows that this model is applicable and has vast prospect in assessing the performance of tetrafluoro skateboard rubber bearings under nitric and sulphuric acids aging condition.

The computational formula of measured vertical stiffness of laminated natural bridge bearings is shown as follows<sup>[12]</sup>:

$$K_v = \frac{P_2 - P_1}{Y_2 - Y_1} \quad (2)$$

Where, P1 is the minimum pressure at third cyclic loading; P2 is the maximum pressure at third cyclic loading; Y1 is the minimum displacement at third cyclic loading; Y2 is the maximum displacement at third cyclic loading.

Fig.7 shows load-vertical stiffness curve of laminated natural bridge bearings. The results show that the damper and thermal aging processing has a relatively little effect on vertical stiffness.

The computational formula of compressive elastic modulus of laminated natural bridge bearings is shown as follows [11]:

$$E_1 = \frac{S_{10} - S_4}{e_{10} - e_4} \quad (3)$$

Where, E1 is a calculated value of compressive elastic modulus;  $S_4$  and  $e_4$  are compressive stress and cumulative compressive strain in the loading stage at 4.0MPa, respectively.  $S_{10}$  and  $e_{10}$  are compressive stress and cumulative compressive strain in the loading stage at 10.0MPa, respectively. The measured compressive elastic modulus of tetrafluoro skateboard rubber bearings is summarized in Table 4.

Tab.4 MEASURED ELASTIC MODULUS COMPARISON OF PTFE SLIDE RUBBER BEARINGS

Specimen	Measured compressive elastic modulus (MPa)
GJZF4200×300×43ZYBZ01	1056.15
GJZF4200×300×43ZYXL020	847.88
GJZF4200×300×43ZYXL040	798.75
GJZF4200×300×43ZYXL060	869.58
GJZF4200×300×43ZYXL080	811.23
GJZF4200×300×43ZYXL100	864.21

## Conclusions

The compression test results show that the specimens after nitric and sulphuric acids aging processing prone to more brittle failure than the standard specimen. Moreover, the steel plate exposed, cracks and other damage phenomena are more serious than the standard specimen.

With the increasing in the aging time and the deepening of the degree of acids aging processing, compressive capacity, ultimate compressive strength and compressive elastic modulus of the tetrafluoro skateboard rubber bearings decreased dramatically.

The test results show that the attenuation trends of ultimate compressive strength and compressive elastic modulus with power function. The attenuation models are acquired by regressing data of experiment with the least square method. The attenuation models conform to reality well which shows that this model is applicable and has vast prospect in assessing the performance of tetrafluoro skateboard rubber bearings under nitric and sulphuric acids aging condition.

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