Online Algorithm for Velocity Estimation in Ultrasonic Doppler Measurement

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Abstract—Ultrasonic Doppler technique is widely used for velocity estimation in medical electronic systems. This technique is signal-processing intensive with an increasing requirement on accuracy, real time and stability. The clutter caused by human tissues contains little information about blood flow velocity. Since conventional algorithms are based on an idealized signal model where the residual clutter is not fully considered, high-performance filters are required for clutter rejection in ultrasonic Doppler measurement. This paper focuses on how to extract the velocity information from ultrasonic echo signals without extra filters. We presented an online algorithm that identified the clutter as unknown parameters instead of filtering. The algorithm does not rely on the performance of extra clutter filters. Simulation results show that this algorithm is simpler and more stable than conventional correlation algorithms.

Keywords—online algorithm; velocity estimation; ultrasonic; Doppler; filter

I. INTRODUCTION

Ultrasonic Doppler technique is widely used in clinical diagnoses, such as cardiology, gynecology and obstetrics. The cardiovascular disease is the leading cause of death that threatens human health. A common symptom of the cardiovascular disease is blood flow abnormality. As one of the most suitable methods for measuring blood flow velocity, ultrasonic Doppler technique has advantages of low cost, no wound and large detection depth. With the rapid development of computer technology and electronic engineering, high-precision, real-time and stable processing has become possible. However, how to extract the velocity information from massive data effectively is still a difficult problem in ultrasonic Doppler measurement.

The conventional algorithms such as auto-correlation algorithm [1], cross-correlation algorithm [2] and maximum likelihood algorithm [3] are based on an idealized signal model. In this model, the residual clutter is not fully considered. The clutter caused by human tissues contains little information about blood flow velocity. High-performance filters are required for clutter rejection. Common examples of linear time-invariant filters were applied, such as finite impulse response filters [4], infinite impulse response filters [5] and autoregression filters [6]. Besides these, many efforts have been made to improve the filtering. C. Demene et al. [7] presented a method for ultrafast ultrasonic imaging based on spatiotemporal singular value decomposition. The method significantly enhanced image contrast. Noting the different spatial characteristics of human tissues and blood flow, C. H. Yu et al. [8] proposed an eigen-based filtering method using Hankel singular value decomposition formulation. The method provided less bias than auto-correlation algorithm. To remove the zero-frequency component, Y. Zhang et al. [9] presented a filter based on empirical mode decomposition. It was proved that the filter had little loss of low blood flow information. Z. Shen et al. [10] suggested a filtering method based on ridge ensemble empirical mode decomposition. The method achieved a high blood-to-clutter energy ratio. Considering the time-varying characteristics of the clutter, various adaptive strategies were proposed [11], [12]. G. Park et al. [13] provided an adaptive method for clutter rejection based on spectral decomposition and tissue acceleration. H. Takahashi et al. [14] presented an adaptive moving-target-indicator filter for clutter rejection. The filter could significantly improve automated identification of the heart wall. In these methods, the clutter was regarded as the interference that should be removed. However, even idealized filters cannot remove the clutter completely due to spectral similarities of the tissue motion and low blood flow. Furthermore, the phase and magnitude of the blood flow signal are changed by filter. The changes will inevitably affect the subsequent processing.

In this paper, we present an online algorithm that identifies the clutter as unknown parameters instead of filtering. The algorithm does not rely on the performance of extra clutter filters. There are three main sections in this paper. Firstly, a typical model of ultrasonic echo signals will be described. Then, we will detail the principle and implementation of the new algorithm. Finally, the algorithm will be evaluated by simulation.

II. SIGNAL MODEL

To extract the velocity information from ultrasonic echo signals, it is necessary to analyze the quantitative relation between them. In this section, we will describe a typical model of the received signal.

The blood flow signal of interest mainly results from the scattering of red blood cells. This signal is so weak that it is easily obscured by the clutter and observation noise. We model the received signal \( x(t) \) as

\[
x(t) = s_b(t) + s_c(t) + \eta(t),
\]

where \( s_b(t) \) is the blood flow signal with a frequency shift due to Doppler effect, \( s_c(t) \) is the clutter and \( \eta(t) \) is observation noise.
noise. A common approach is assuming that the clutter is caused by static tissues [15]. Therefore, the clutter has the same frequency as the excitation. A typical excitation in ultrasonic Doppler measurement is periodic pulses. Due to the use of digital processing system, a discrete-time data set can be sampled. Let \( x[n,n_{prf}] \), \( s[n,n_{prf}] \), \( s_0[n,n_{prf}] \) and \( e[n,n_{prf}] \) denote the values of \( x(t) \), \( s(t) \), \( s_0(t) \) and \( e(t) \) at the \( n \)-th sampling moment in the \( n_{prf} \)-th period. If the excitation pulses are sinusoidal, then

\[
s_b[n, n_{prf}] \approx A_b \sin \left( 2\pi f_T n_s - 4\pi f_{prf} n_{prf} \nu / c + \phi_0 \right),
\]

(2)

\[
s_c[n, n_{prf}] \approx A_c \sin \left( 2\pi f_T n_s + \phi_i \right),
\]

(3)

where \( A_b \) and \( A_c \) represent the amplitude attenuation due to propagation losses, \( \phi_0 \) and \( \phi_i \) are the phase shifts that are related to the detection depths, \( f_T \) is the center frequency of the transmitted pulses, \( T_s \) is the sampling interval, \( T_{prf} \) is the pulse repetition period, \( \nu \) is the blood flow velocity, and \( c \) is the speed of sound.

Finally, the sampling value could be expressed by

\[
x[n, n_{prf}] = s_b[n, n_{prf}] + s_c[n, n_{prf}] + e[n, n_{prf}]
\approx A_b \sin \left( 2\pi f_T n_s - 4\pi f_{prf} n_{prf} \nu / c + \phi_0 \right) + A_c \sin \left( 2\pi f_T n_s + \phi_i \right) + e[n, n_{prf}].
\]

(4)

In summary, we model the sampling value as the summation of the blood flow signal, the clutter and observation noise. The blood flow signal has a frequency shift that is proportional to the velocity due to Doppler effect.

III. SIGNAL PROCESSING ALGORITHM

The previous section analyzed the quantitative relation between the blood flow velocity and the received signal. The problem now is how to estimate the velocity \( \nu \) based on 2-D data set \( x[n,n_{prf}] \). This section will detail the principle and implementation of the new algorithm.

A. Algorithm Principle

We wish to maximize the probability density function \( p(x;\nu) \) over \( \nu \). Consider the velocity estimator

\[
\hat{\nu} = \arg \max_\nu \left[ p(x;\nu) \right].
\]

(5)

Assume that \( e[n, n_{prf}] \) is white Gaussian noise. Then,

\[
J = \sum_{n=0}^{N_{prf}-1} \frac{1}{N_s} \sum_{n=0}^{N_s-1} e[n, n_{prf}] \exp \left( 2\pi i f_{prf} T_s n_s \right).
\]

(6)

Thus, the probability density function can be written as

\[
p(x;\nu) = \left( \pi \sigma^2 / N_s \right)^{N_{prf}/2} \exp \left( -N_s J / \sigma^2 \right).
\]

(8)

Now we are equivalently minimizing \( J \) in maximizing \( p(x;\nu) \). From (5),

\[
\hat{\nu} = \arg \max_\nu \left[ p(x;\nu) \right] = \arg \min_\nu (J).
\]

(9)

Let \( f = 2\nu f_{prf} T_s / c \), \( \theta_1 = 0.5A_b \cos \phi_0 \), \( \theta_2 = 0.5A_b \sin \phi_0 \), \( \theta_3 = 0.5A_c \cos \phi_i \), \( \theta_4 = 0.5A_c \sin \phi_i \) and

\[
y[n] = \frac{1}{N_s} \sum_{n=0}^{N_s-1} x[n,n] \exp \left( 2\pi i f_{prf} T_s n_s \right).
\]

(10)

The real part and imaginary part of \( y[n] \) are denoted by \( y_R[n] \) and \( y_I[n] \) respectively. Then, we have

\[
J = \sum_{n=0}^{N_{prf}-1} \left( y_R[n] - \theta_4 \sin (2\pi f)n - \theta_3 \cos (2\pi f)n \right)^2 + \sum_{n=0}^{N_{prf}-1} \left( y_I[n] - \theta_1 - \theta_2 \cos (2\pi f)n - \theta_0 \sin (2\pi f)n \right)^2.
\]

(11)

J is a function of \( f \), \( \theta_1 \), \( \theta_2 \), \( \theta_3 \) and \( \theta_4 \). \( f \) is proportional to the velocity. Since \( J(f+1) = J(f) \), we only need to consider \(-0.5 < f \leq 0.5 \). Besides \( f \) of interest, \( \theta_1 \), \( \theta_2 \), \( \theta_3 \) and \( \theta_4 \) are all unknown parameters. Consider the parameters that minimize \( J \), denoted by

\[
\hat{\theta} = \left[ \hat{\theta}_1, \hat{\theta}_2, \hat{\theta}_3, \hat{\theta}_4 \right]^T.
\]

The superscript T represents matrix transpose.

Setting the partial derivatives of \( J \) to zero, we have

\[
\frac{\partial J}{\partial \theta} |_{\theta=0} = 0.
\]

(13)

That is

\[
\left( \begin{array}{ccc}
N_{prf} & 0 & \sum_{k=0}^{N_{prf}-1} \cos \sum_{h=0}^{N_{prf}-1} \sin \\
0 & N_{prf} & \sum_{k=0}^{N_{prf}-1} \sin \sum_{h=0}^{N_{prf}-1} \cos \\
\sum_{k=0}^{N_{prf}-1} \cos \sum_{h=0}^{N_{prf}-1} \sin & 0 & N_{prf} \\
\sum_{k=0}^{N_{prf}-1} \sin \sum_{h=0}^{N_{prf}-1} \cos & 0 & N_{prf}
\end{array} \right) \hat{\theta} = \left( \begin{array}{c}
\sum_{k=0}^{N_{prf}-1} y_k \cos - \sum_{k=0}^{N_{prf}-1} y_k \sin \\
\sum_{k=0}^{N_{prf}-1} y_k \sin + \sum_{k=0}^{N_{prf}-1} y_k \cos \\
\sum_{k=0}^{N_{prf}-1} y_k \sin + \sum_{k=0}^{N_{prf}-1} y_k \cos \\
\sum_{k=0}^{N_{prf}-1} y_k \sin + \sum_{k=0}^{N_{prf}-1} y_k \cos
\end{array} \right).
\]

(14)
If \( f \neq 0 \), then solving (14) yields \( \hat{\theta} \). Substituting \( \hat{\theta} \) in (11) and letting \( z[n] = y[n] - \sum y[n]/N_{\text{fft}} \), we have

\[
J_{\theta} = \frac{1}{N_{\text{fft}}} \frac{1}{N_{\text{fft}}} \sum_{n=0}^{N_{\text{fft}}-1} \sum_{n'=0}^{N_{\text{fft}}-1} \sum_{n''=0}^{N_{\text{fft}}-1} \frac{1}{N_{\text{fft}}} \exp(-i2\pi fn) \right]^2.
\]  

(15)

Let \( Z(f) \) denote the Fourier transformation of \( z[n] \). If \( N_{\text{fft}} \) is large enough, then

\[
J_{\theta} \approx \frac{1}{N_{\text{fft}}} \frac{1}{N_{\text{fft}}} \sum_{n=0}^{N_{\text{fft}}-1} \sum_{n'=0}^{N_{\text{fft}}-1} \sum_{n''=0}^{N_{\text{fft}}-1} \frac{1}{N_{\text{fft}}} \exp(-i2\pi fn) \right|^2.
\]  

(16)

From (9),

\[
\hat{\vartheta} = \arg \min \left\{ J \right\} = \frac{c}{2f_cT_{\text{fft}}} \arg \min \left\{ J_{\theta} \right\} = \frac{c}{2f_cT_{\text{fft}}} \arg \max \left| Z(f) \right|.
\]  

(17)

However, the estimator is not always feasible because (15) requires \( f \neq 0 \). Noting that \( |Z(0)| = \sum z[n] = 0 \), the estimator is invalid if \( f \approx 0 \). Hence, revise (17) as

\[
\hat{\vartheta} = \frac{c}{2f_cT_{\text{fft}}} \arg \max \left| Z(f) \right| + \gamma \delta(f),
\]  

(18)

where \( \gamma \) is a constant selected by user and \( \delta \) is the Dirac function.

In summary, the velocity estimator of the new algorithm is

\[
\hat{\vartheta} = \frac{c}{2f_cT_{\text{fft}}} \arg \max \left| Z(f) \right| + \gamma \delta(f),
\]  

(19)

where \( c \) is the speed of sound, \( f_c \) is the center frequency of transmitted pulses, \( T_{\text{fft}} \) is the pulse repetition period, \( \gamma \) is a constant selected by user, \( \delta \) is the Dirac function, \( Z(f) \) is the Fourier transform of \( z[n] \) and

\[
z[n] = \frac{1}{N_{\text{fft}}} \sum_{n=0}^{N_{\text{fft}}-1} \left[ x[n]\sum_{n'=0}^{N_{\text{fft}}-1} x[n',n] \right] \exp(i2\pi fnT_{n}).
\]  

(20)

\section{Algorithm Implementation}

The above batch algorithm processes all the data at once. It means that users have to wait for all the available data, or compute the preceding data repeatedly. To reduce time and calculation work, we process the samples sequentially in time.

If we received the data of the \( k \)-th period just now, then compute \( y[k-1] \) based on the new data \( x[n,k-1] \) by

\[
y[k-1] = \frac{1}{N_{\text{fft}}} \sum_{n=0}^{N_{\text{fft}}-1} x[n,k-1] \exp(i2\pi fnT_{n}).
\]  

(21)

Letting \( \gamma = 0 \), the estimator \( \vartheta(k) \) is

\[
\vartheta(k) = \frac{k+1}{k} \mu(k) + \frac{1}{k} \sum_{n=0}^{k-1} y[n,k] - \vartheta(k-1)
\]  

(24)

Introduce intermediate variables \( \vartheta(k) \) and \( u(k) \). Let

\[
\vartheta(k) = \frac{k+1}{k} \mu(k) + \frac{1}{k} \sum_{n=0}^{k-1} y[n,k] - \vartheta(k-1),
\]  

(22)

\[
u(k) = \frac{k+1}{k} \mu(k) + \left[ \exp \left( -i2\pi f_{n} \right) \right].
\]  

(25)

Letting \( Z^{(k)}(f) \) denote \( Z(f) \) obtained from the first \( k \) periods, we have

\[
Z^{(k)}(f) = Z^{(k-1)}(f) + \frac{1}{k} \left[ \exp \left( -i2\pi f_{n} \right) \right].
\]  

(26)

Summarize the recursive procedures as follows:

\begin{enumerate}
  \item Initialize the variables: \( k = 0, \vartheta(0) = 0, u(0) = 0, Z^{(0)}(f) = 0 \);
  \item Increase the index \( k \) by 1 and wait for new data;
\end{enumerate}
Step 3. Compute \( y[k-1] \) based on the most recent data \( x[n_k,k-1] \) by (21);

Step 4. Update the variables \( y^{(k)}, \mu^{(k)} \) and \( Z^{(k)}(f) \) by (24)(25)(26);

Step 5. Compute \( Z^{(k)}(f) \) and select a proper \( \gamma \);

Step 6. Compute \( \hat{v}\) by (19), and then return to Step 2 until no more data are sampled.

IV. SIMULATION RESULTS AND DISCUSSION

In this section, we will compare the new algorithm with conventional correlation algorithms by simulation. Simulate echo signals with the toolkit Field II, and then compute the velocity estimators separately.

Firstly, set sound field parameters. The speed of sound in human tissues is 1540m/s. The excitation is sinusoidal periodic pulses with the center frequency of 5MHz. There are 32 pulses with intervals of 100μs. The sampling interval is 25ns. The radius of the vessel is 4mm and the vessel is at the depth of 30mm with a 45° angle to the ultrasonic beam. A 128-element ultrasonic phased array probe is used. The elements are 0.15mm width and 5mm length with kerfs of 0.03mm. The speed of sound in ultrasonic phased array probe is 1540m/s. The excitation is sinusoidal periodic pulses with the center frequency of 5MHz. There are 32 pulses with intervals of 100μs. The sampling interval is 25ns. The radius of the vessel is 4mm and the vessel is at the depth of 30mm with a 45° angle to the ultrasonic beam. A 128-element ultrasonic phased array probe is used. The elements are 0.15mm width and 5mm length with kerfs of 0.03mm. The speed of sound in ultrasonic phased array probe is 1540m/s. The excitation is sinusoidal periodic pulses with the center frequency of 5MHz. There are 32 pulses with intervals of 100μs. The sampling interval is 25ns. The radius of the vessel is 4mm and the vessel is at the depth of 30mm with a 45° angle to the ultrasonic beam. A 128-element ultrasonic phased array probe is used. The elements are 0.15mm width and 5mm length with kerfs of 0.03mm. The intensity ratio of red blood cells to static tissues is 0.1. The new algorithm identifies the clutter as unknown parameters instead of filtering, and does not rely on the performance of extra filters. To reduce time and calculation work, the sequential processing is recommended.

In summary, we compare the algorithms in three aspects.

1) **Accuracy.** All the algorithms work well.
2) **Stability.** Correlation algorithms are sensitive to the clutter. The new algorithm which does not rely on the performance of extra filters is the most stable one.
3) **Simplicity.** Compared with the conventional correlation algorithms, the new algorithm is easier to implement.

V. CONCLUSION

This paper focused on how to extract the velocity information from ultrasonic echo signals without extra filters.

An online algorithm was presented. Since the algorithm identifies the clutter as unknown parameters instead of filtering, it does not rely on the performance of extra clutter filters. To reduce time and calculation work, the sequential processing is recommended.

Compared with the conventional correlation algorithms, the new algorithm is simpler and more stable.

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