

Optimization of Component Characteristics in EMI Filter Using CST MWS

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Abstract. This paper is devoted to the design of electromagnetic interference (EMI) filter circuit. In particular, the component parameters are carefully considered and optimized in assistance of 3-D electromagnetic software CST MWS. What distinguishes this paper from others is that an overall model of the filter instead of isolated components is constructed.

Introduction

To meet electromagnetic compatibility (EMC) requirements, EMI filter is of great significance. However, the research of the component characteristics has been temporarily out of the focus, which deserves equivalent concern. To fill the void, this paper presented here aims to the optimize the filter design in terms of component parameters using CST MWS. This paper firstly introduces a preliminary filter circuit to be improved. X capacitor, Y capacitor and common-mode(CM) inductor are modeled in CST MWS. The components are modified and the filter is constructed which proves to have good filtering performance.

Preliminary EMI filter circuit

In search of the most suitable parameters, it would be more convenient to start from the filter prevailing in the market. A typical filter circuit is proposed as the preliminary design(Fig.1) .

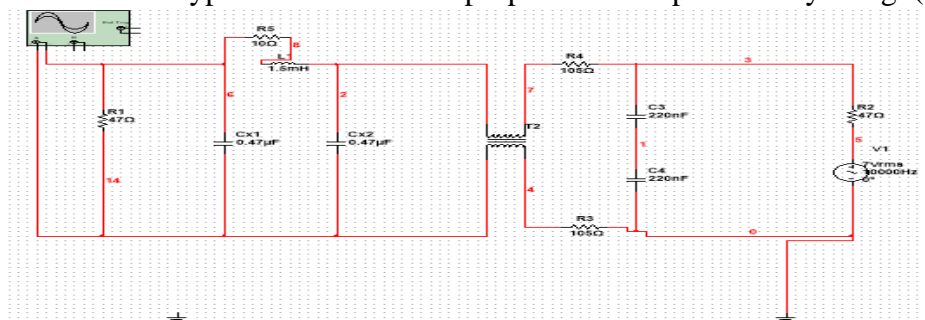


Fig.1 The preliminary filter design with typical component parameters.

Capacitor Modeling

X Capacitor Modeling.

The actual capacitor(Fig.2) is manufactured with conductive film layer inside. For convenience,the model is simplified to be filled with internal normal conductor. Two thin dielectrics are attached to the normal conductor,covered with identical pieces of perfect conductor outside,from which the wires are led with length 5mm each. Measurement is carried out precisely to simulate the actual capacitor. The distance between the plates $d=0.014\text{m}$,the plate area $A=0.5e^{-4}$

m^2 . According to the formula: $C = \frac{\epsilon_r \cdot S}{4\pi k d}$, Relative permittivity $\epsilon_r=1.04e^7$. Thus the capacitor is modeled(Fig.3).



Fig.2 X capacitor prototype and the inner structure

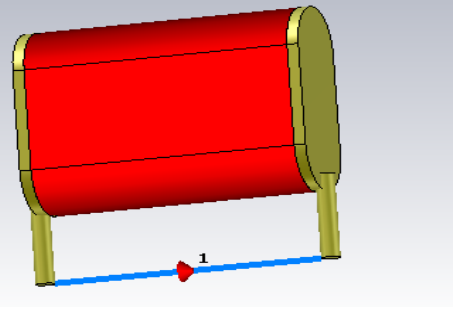


Fig.3 X capacitor model

Analysis and Result of X Capacitor.

The background substance is selected as air and is extended 20 mm outward from the model in three directions. The external boundary is set as short-circuit boundary $E_t=0$. Default mesh dissection is adopted. Z-parameters is depicted in Fig.4, which contains oscillation and energy divergence. Post-process the data by adopting the default AR filter setting and the result is illuminated in Fig.5.

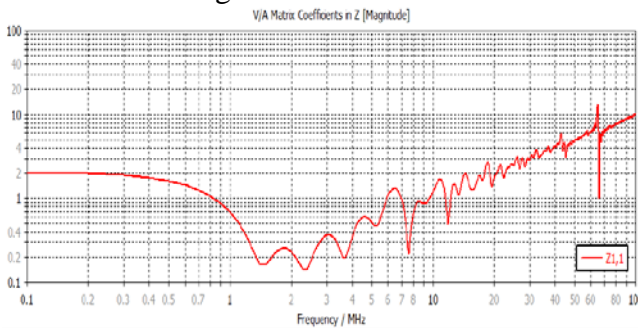


Fig.4 Z-parameters of X capacitor

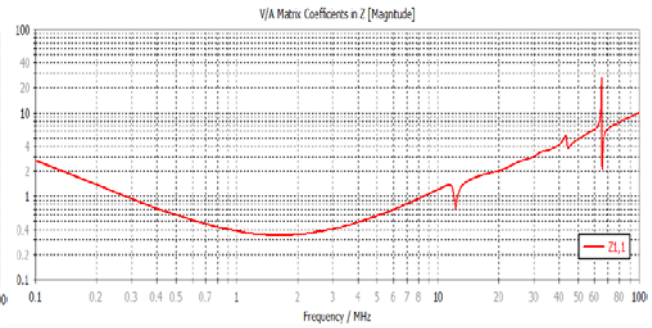


Fig.5 Z-parameter after AR filter of X capacitor

3 marks are attached to the curve as below(Fig.6). The impedance at 0.2 MHz is 1.37 Ohm, thus the capacitance is 0.58 uF. The impedance is 3 Ohm at 30MHz, so the inductance value is 15.9 nH. As the dielectric loss factor of the second mark is 0.001, the impedance is 0.343 Ohm at 1.66 MHz. The RLC values in series connection are determined.

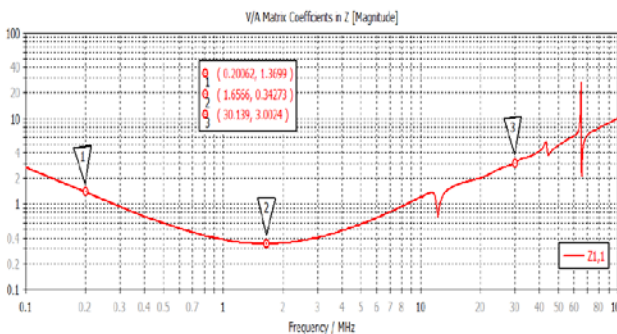


Fig.6 Z-parameter after AR filter of X capacitor attached with marks

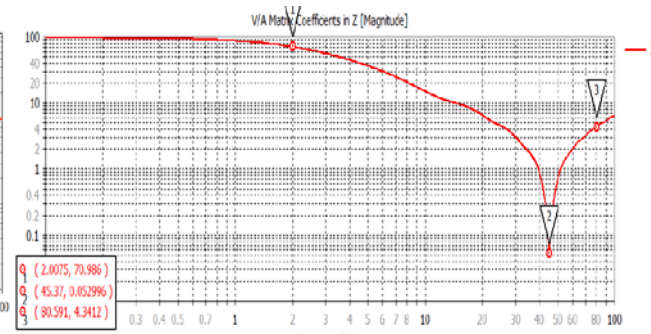


Fig.7 Z-parameters of Y capacitor

Y capacitor Modeling and Analysis.

Similarly, Y capacitor is modeled. The distance between the two plates $d=0.005\text{m}$, the plate area $A=0.5e^{-6}\text{m}^2$, relative permittivity $\epsilon_r=1.13e^5$. Attach 3 marks to the Z-parameter curve and we get Fig.7. The impedance at 2 MHz is 71.0 Ohm, thus the capacitance is 0.001uF. The impedance is 4.3 Ohm at 80MHz, so the inductance value is 8.55 nH. As the dielectric loss factor of the second mark is 0.001, the impedance is 0.05 Ohm at 45.37 MHz. The RLC values in series connection are determined.

Common-mode inductor modeling

Inductor Modeling.

As is shown in Fig.8, the common-mode inductor is modeled. The dimensions and the material are set the same as the prototype. Two identical coils with 5 turns each are wound around the core in reverse symmetrically.

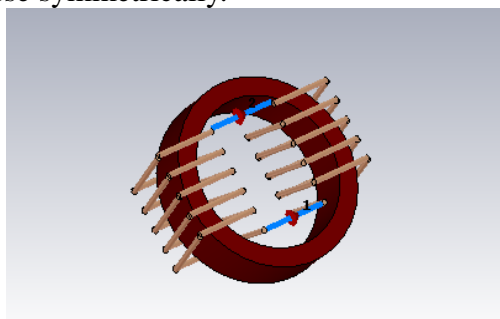


Fig.8 3-D model of Inductor

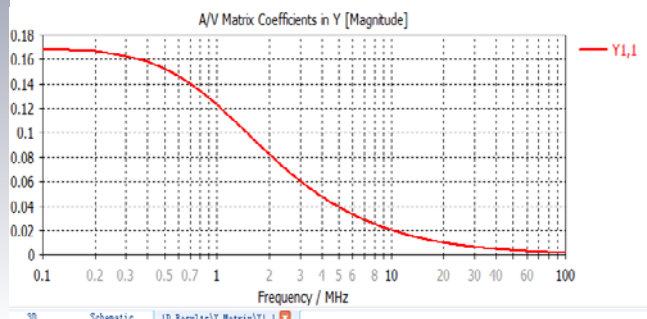


Fig.9 Y versus frequency in condition of differential-mode interference

Differential-mode Interference.

Two ports are defined at the ends of both coils and DM interference analysis is conducted. Z1-1 does not represent the impedance curve due to the existence of the ports. Thus Z-parameter (the reciprocal of Y1-1) is calculated by EXCEL after Y1-1 is obtained and exported (Fig.10)

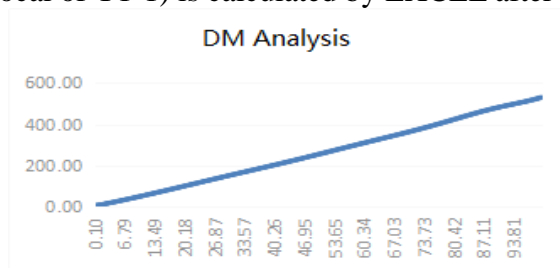


Fig. 10 1/Y1-1 versus frequency in condition of differential-mode interference

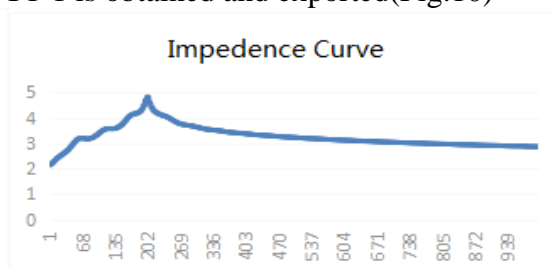


Fig.11 Impedance Curve of CM analysis

Common-mode Interference.

CM interference analysis of the CM inductor is conducted. The PCB material is normal dielectric with dielectric constant is 4.5. The bottom layer of PCB is perfect conductor serving as ground. 1/Y1-1 is obtained by EXCEL (Fig.11).

Modeling of circuit

DM modeling & Analysis.

To reduce the effect of mutual coupling, the circuit model is improved repeatedly till the ultimate one with much simplified connection is put forward (Fig.12). S2-1 of DM modeling is shown in Fig.13, indicating excellent filtering performance.

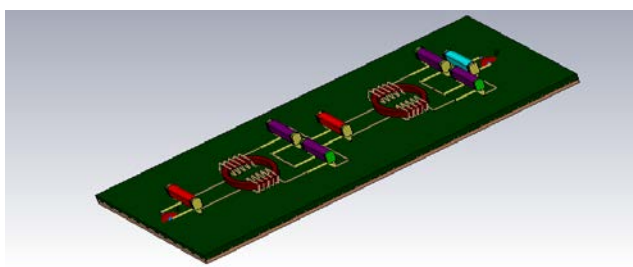


Fig.12 circuit model for DM mode modeling

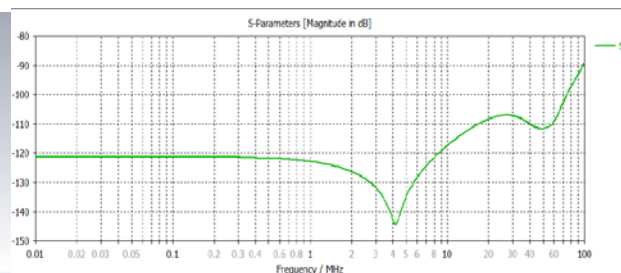


Fig.13 S2-1 of DM modeling

CM mode modeling & analysis.

For CM interference, two ports of the circuit are connected together (Fig.14). S2-1 of CM modeling is shown in Fig.15, indicating excellent filtering performance.

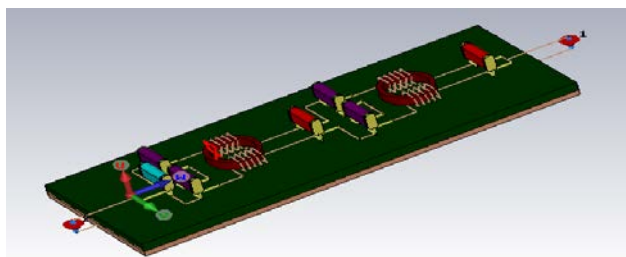


Fig.14 circuit model for CM mode modeling

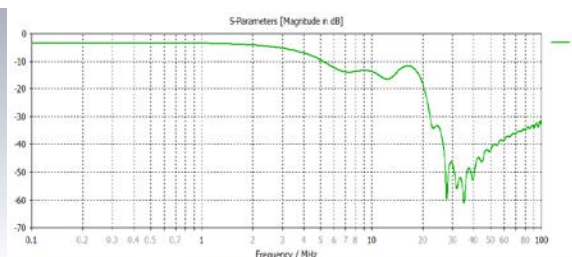


Fig.15 S2-1 of CM modeling

Conclusion

This paper focuses on the design of EMI filter in terms of component parameters using CST MWS. Capacitors and CM inductor have been modeled. The components are mounted on the PCB model in an appropriate way avoiding the impact of mutual coupling. The parameters are found to be the most suitable for filtering. The result analysis demonstrates that the filter designed in this paper functions well.

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