

Dynamic Analysis of Squeeze Piezo Printhead Using Reduced Frequency Model

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Abstract. The dynamic characteristics of squeeze piezo printhead are studied using reduced frequency model for inks with different viscosity. While piezo inkjet mainly applies in paper printing and graphic output, many new applications have emerged in the last few years. These new applications involve inks with high viscosity. Ink viscosity is a key material parameter in printhead design. In order to take viscous damping into account, reduced frequency model is applied to model the printhead fluid cavity. Squeeze piezo printhead models with different inks (viscosity range from 20 cps to 110 cps) are built using software ANSYS15.0. Meniscus velocity and pressure at the nozzle entrance excited by frequency from 10 KHz to 200 KHz are calculated. Meantime, the velocity and pressure distribution around the first resonant frequency (which is 21250 Hz in the paper) are also calculated. The results reveal that both meniscus velocity and pressure decrease with increasing viscosity. It is notable that ink viscosity affects the printhead dynamic response significantly near resonant frequency. When the exciting frequency is far from resonant frequency, the influence of viscosity is small. The reduced frequency model is a powerful tool for the design optimization of the piezo printhead.

1. Introduction

Piezo printing has major applications in paper printing and graphic output for now. However, more and more researchers are getting interested in using piezo printing to manufacture complex components for applications in fields such as displays [1], plastic electronics [2], tissue engineering [3, 4]. A significant and fundamental difference between these new applications and the traditional application of paper printing is that the “ink” used in these new applications always have more complex fluid properties such as non-continuous, non-Newtonian and highly viscous. In order to study the printing theory and develop new piezo printhead used in the emerging fields [4], it is essential to capture and control the flow phenomena in piezo printhead during inkjet process.

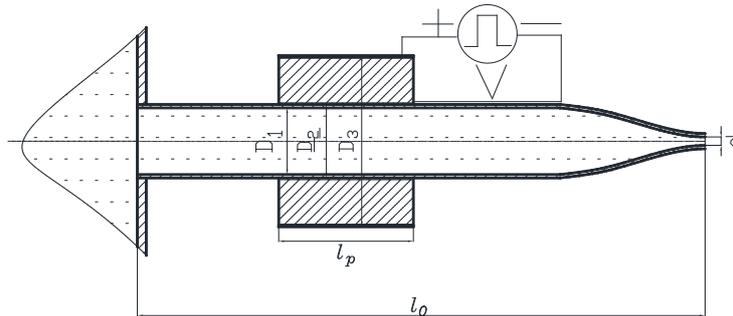
Many studies about the theme are published and most are carried out through experimental method [5-7]. Because piezo printhead generally has small dimension, the experiments are always expensive. Meantime, piezo ink printing involves several physical processes [8]. It is hard to conclude useful rule for different ink printing from experiments.

Computer simulation is also a powerful method to study piezo printhead [9]. Because physical processes including piezoelectricity, structure dynamics, acoustics and fluid dynamics are involved. The complete simulation model must be multi-fields coupled. While coupled model generally is hard to build and time-consuming to solve, sequential method, which featured that results from one fields are input as loads for the next fields, are popular and appropriate under most circumstances.

There are several models to simulate the generation and propagation of pressure wave in the printhead fluid cavity. Full Navier-Stokes equation, which is the most fundamental and execute model theoretically, is very time consuming and few researchers try to apply it. Pure acoustic theory is much simpler, but the viscous damping effects are neglect, while the viscous damping is essential for small section cavity flow. Reduced frequency model, which is also known as narrow channel

theory, is a simplified version of more general Navier-Stokes equation in the printhead analysis. Features of very small section dimension compared to axial one is taken into account. The theory is first developed for calculating acoustics in narrow gap [10]. The simplified model is much cheaper than general Navier-Stokes equation for narrow channel flow. Especially the viscous damping of the ink is taken into account and the resulted fluid cavity flow field generally is more execute compared with pure acoustic simulation.

In this paper, the piezo printhead are simulated using sequential coupled method. Structure FE model (including Piezo actuator and lining) is built and solved firstly. The resulted inner wall displacement is input as load in the next reduced frequency fluid cavity simulation. With different exciting frequency, pressure and velocity distribution in the fluid cavity are calculated. Pressure at the nozzle entrance (P_n) and meniscus velocity (V_m) are most important index in printhead design. Effects of the fluid viscosity on P_n and V_m are also studied. The whole simulation is carried out using software ANSYS 15.0.



* $D_1=0.5mm$, $D_2=0.508mm$, $D_3=1.516mm$, $l_0=24mm$, $l_p=10mm$, $d=0.05mm$

Fig.1 Structure of the studied piezo printhead

3. Simulation strategy and FE model

Structure of the squeeze mode piezo printhead is shown in Fig. 1. Glass lining filled with ink is surrounded by radially polarized piezoelectric ceramic PZT-5H ring. Both inner and outer surface of PZT-5H ring are covered by conductive layer as electrode, which is used to apply exciting electric field. Because the conductive layers are much thinner than the PZT-5H ring, it is reasonable to neglect the layers for simplification. The material properties of PZT-5H, glass lining and ink are shown in Table 1.

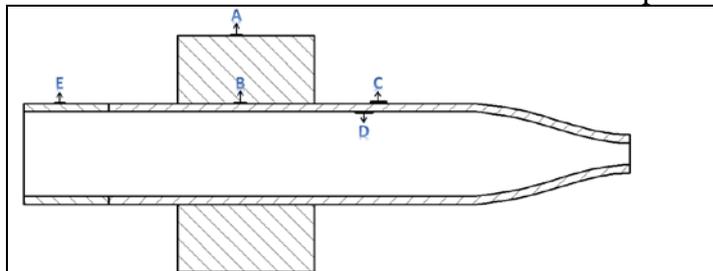
Table. 1 Material Properties used in the study

PZT-5H	Elastic Modulus c	$\begin{bmatrix} 127 & 80.2 & 84.7 & 0 & 0 & 0 \\ 80.2 & 127 & 84.7 & 0 & 0 & 0 \\ 84.7 & 84.7 & 117 & 0 & 0 & 0 \\ 0 & 0 & 0 & 23 & 0 & 0 \\ 0 & 0 & 0 & 0 & 23 & 0 \\ 0 & 0 & 0 & 0 & 0 & 23.5 \end{bmatrix} \times 10^9 \text{ pa}$
	Piezoelectric Matrix e	$\begin{bmatrix} 0 & 0 & -6.23 \\ 0 & 0 & -6.23 \\ 0 & 0 & 23.2 \\ 0 & 17.03 & 0 \\ 17.03 & 0 & 0 \\ 0 & 0 & 0 \end{bmatrix} \text{ C/m}^2$
	Dielectric Constant ϵ	$\begin{bmatrix} 1.5 & 0 & 0 \\ 0 & 1.5 & 0 \\ 0 & 0 & 1.3 \end{bmatrix} \times 10^{-8} \text{ F/m}$
Glass	Elastic Modulus c	$7.01 \times 10^{10} \text{ pa}$
	Poisson Ratio	0.17
	Density	2203 kg/m^3
Ink	Sound Velocity	1483 m/s
	Density	998 kg/m^3
	Viscosity	$20 \times 10^{-3} \sim 110 \times 10^{-3} \text{ pa} \cdot \text{s}$

In order to simplify the simulation, a printhead structure simulation is carried out first. The resulted inner wall displacement is used as load input for next fluid cavity RF model.

ANSYS APDL introduced the advanced RF model in version 15.0 and the platform is used in this study. As shown in Fig. 2, coupled field element SOLID226 and structure element SHELL 281 are used to simulate the PZT-5H ring and glass lining respectively. The FE model and boundary conditions for piezo structure analysis show in Fig. 2(a) and Table 2 respectively.

Table. 2 FE model BCs of piezo structure analysis

	A	B	C
	VOLT=0V	VOLT=12V	
	Free	Free	Free
	Coupled	Coupled	
	VOLT	VOLT	
	D	E	
	Free	Clamped	

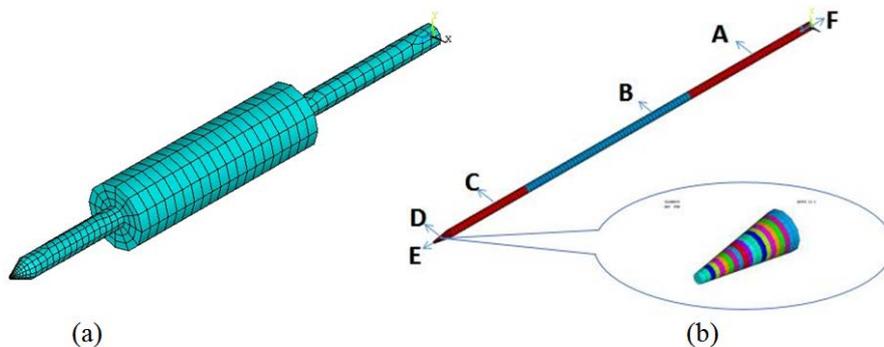


Fig. 2 FE models for structure simulation (a) and the fluid cavity (b).

Element FLUID220 is selected for simulate the fluid domain. It is noteworthy that channel shape and dimension need to be specified explicitly using material properties with RF model in ANSYS. Because the nozzle has a conical shape and its radius is different along longitudinal direction. In order to model the nozzle precisely, layer of 0.15 mm is used to divide the conical into a series of cylinder part, which are simulated with corresponding radius (Fig. 2(b)). Reduced frequency model is flagged

on. FSI interface and inner wall radial displacement calculated in the former structure analysis are applied on the interface. Because the radius of fluid cavity is very small, gravity is ignored in the model and reservoir has much larger volume than the fluid cavity. The boundary conditions of both interface (surface F) and the meniscus are set as zero pressure (Table. 3).

Table. 3 Boundary Conditions of Fluid Cavity RF models

Surface A, C and D	Surface B	Surface E and F
$U_Y = 0; U_Z = 0$ $ROT_X = 0; ROT_Y = 0;$ $ROT_Z = 0$ SFI flag on	$U_X = Disp_Wall; U_Y = 0; U_Z = 0$ $ROT_X = 0; ROT_Y = 0; ROT_Z = 0$ SFI flag on	PRES = 0

※ All the displacement are specified in cylinder coordinate shown in Fig. 2(b).

4. Result and analysis

4.1 Results of structure simulation

The printhead structure simulation is carried out firstly. Deformation of the structure excited by 12V voltage is calculated (as shown in Fig. 3). Inner wall radial displacement $Disp_Wall$ is key quantity as load input in the next RF simulation. In this case, the $Disp_Wall$ is 14 nm.

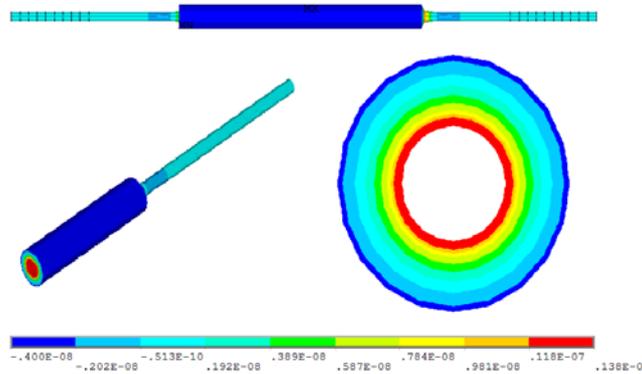


Fig. 3 Printhead deformation excited by 12V voltage

The paper is focused on the topic how viscosity affect the printhead dynamic properties and ink viscosity has negligible influence on the structure deformation. Therefore, in the following simulation, constant inner wall displacement $Disp_Wall$ is applied.

4.2 Results of fluid simulation

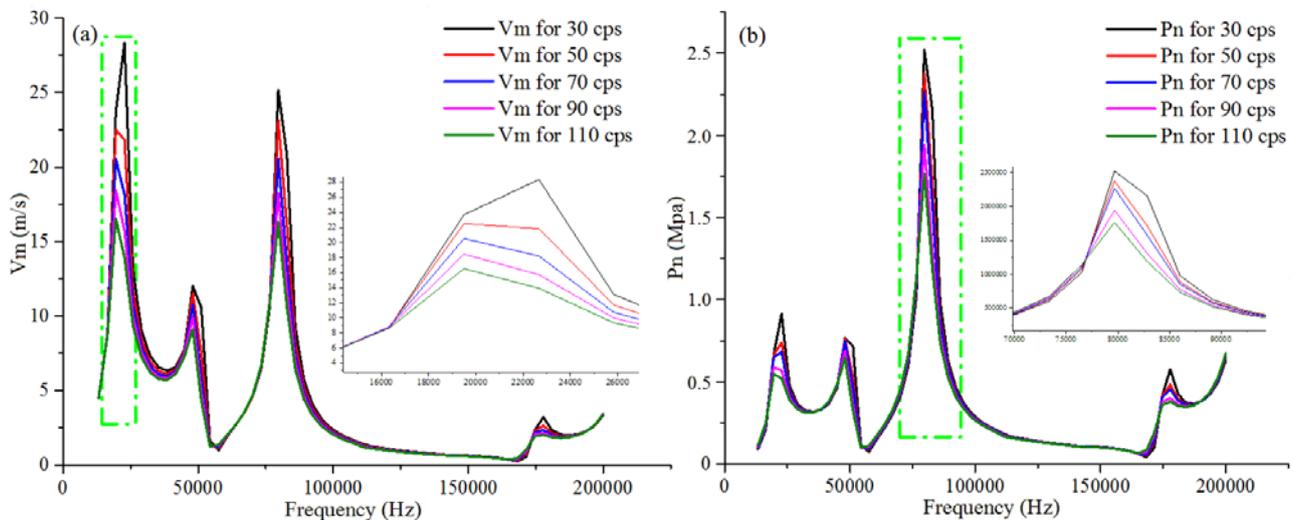


Fig. 4 Relationships of V_m , P_n and frequency

Harmonic simulations for various viscosities (from 20 cps to 110 cps with step 10) are carried out. The sweeping frequency is from 10K Hz to 200K Hz, which is the typical piezo printhead working

frequency. Through the simulation, the frequency response of meniscus velocity V_m and pressure at the nozzle entrance P_n for various are calculated (Fig. 4).

It is obvious that the viscosity has the most significant impact on both V_m and P_n around resonant frequency. When the exciting frequency is far from resonant frequency, the V_m and P_n are almost the same for all the simulated viscosity. However, in order to enhance piezo printhead performance, actual working frequency is always selected around resonant frequency.

Table. 4 V_m and P_n for various viscosities at the first resonant frequency (21250 Hz)

Viscosity/cps	20	30	40	50	60
V_m /(m/s)	51.65	41.14	34.28	29.53	26.31
P_n /pa	645963	502045	404167	350507	302224
Viscosity/cps	70	80	90	100	110
V_m /(m/s)	23.93	21.90	20.17	18.67	17.38
P_n /pa	265638	237961	209755	192616	174792

It is essential to get insight how viscosity affect the value of V_m and P_n around resonant frequency. A second harmonic analysis around the first resonant frequency (from 10K Hz to 40K Hz) is carried out to capture the variation tendency details of V_m and P_n . And the detailed frequency response graphs (Fig. 5) show that values of both V_m and P_n decrease with increasing ink viscosity.

Since both V_m and P_n curves for large viscosity are flat compared to ones for small viscosity. It is safe to say that through low viscous ink can achieve higher V_m and P_n , the performance are more sensitive to exciting frequency and working frequency and exciting wave shape must be selected carefully.

Meantime, viscosity did not affect the resonant frequency (21250 Hz for this case). Values of V_m and P_n for different viscosity at the resonant frequency are listed in the Table 5. One would expect the viscosity to affect the damping (which decreases the values of V_m and P_n), but not the resonant frequency. Because the simulation neglect glass lining in the RF model, it is notable the resulted V_m and P_n are larger than the real values. The result can be used as upper limits.

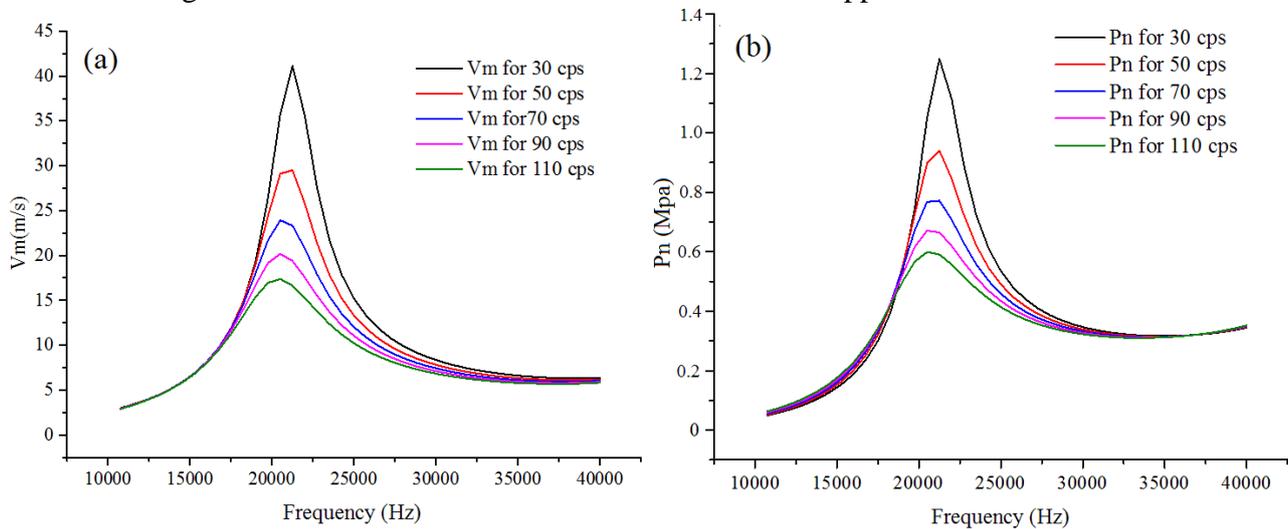


Fig. 5 Meniscus velocity (a) and pressure at nozzle entrance (b) frequency responses around the first resonance frequency

4.3 Results for velocity and pressure distribution near resonant frequency

The details of velocity (v) and pressure (p) distribution in the piezo printhead fluid cavity are helpful for printhead design and optimization. From the former harmonic analysis, it can be concluded that the meniscus achieves largest velocity value when the exciting load is at the first resonant frequency, which is 21250 Hz for the studied printhead. Velocity and pressure distribution near 21250 Hz for different viscous ink are presented in the following analysis.

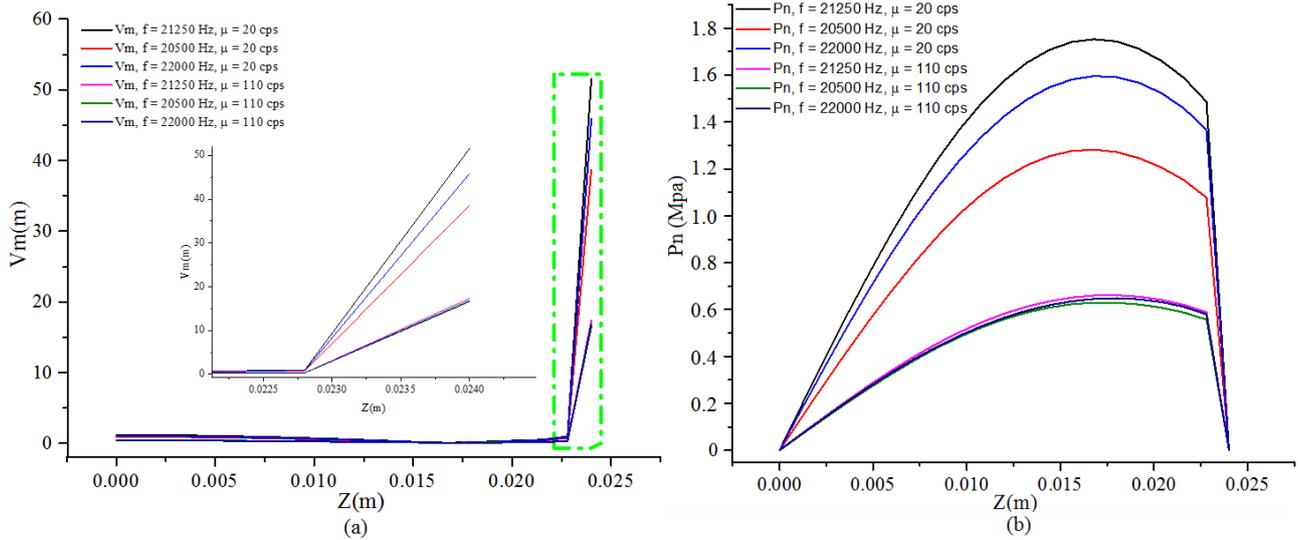


Fig. 6 Curves of V_m - Z (a) and P_n - Z (b)

A coordinate as shown in Fig. 2 is specified in the following analysis. Z -axis coincides with the central axis of the fluid cavity. From the curves of P - z and V - z (Fig. 6) at different viscosity and exciting frequency, it is obvious that neither ink viscosity nor exciting frequency, which is near resonant point, affects p and V tendency along Z direction. Only p and V values are affected by ink viscosity and exciting frequency. Viscosity affects the V , and p significantly, especially within the nozzle. Both V and P decrease with increasing viscosity. For high-viscosity case, the values of V and p are not as sensitive to the exciting frequency as for low-viscosity case (also shown in Fig. 5(b)). Both V and p change dramatically within the nozzle. Contour of V and p are presented in Fig. 7.

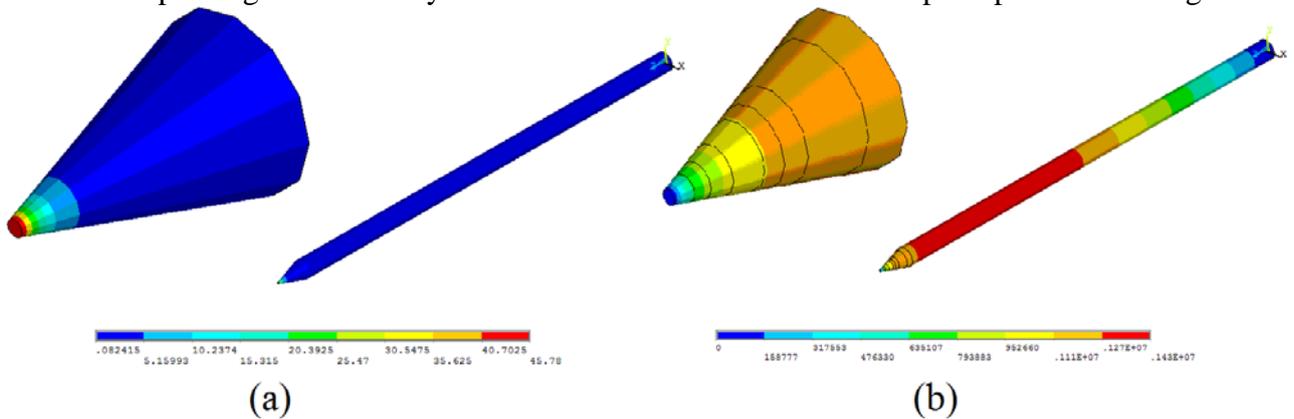


Fig. 7 Contours of V (a) and P (b)

5. Conclusion

This research has built a reduced frequency simplified simulating model for the squeeze mode piezo printhead. The simplified model is then used to study the dynamic characteristics of the printhead fluid cavity. Various inks with different viscosity are simulated to study how viscosity affects the fluid cavity frequency response. Meniscus velocity V_m and pressure at nozzle entrance P_n are key quantities in the research and they are calculated using the simplified model. The distribution of pressure and velocity near the resonant frequency are also presented in paper. Simulation results reveal the meniscus velocity and pressure at nozzle entrance are affected by viscosity near resonant frequency significantly and it is important to take a full account of viscosity when one designs a new piezo printhead. The presented model is a powerful tool to evaluate the viscosity effect and it also has great potential to be extended for the design optimization of the piezo printhead.

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