

Crystal Plasticity Finite-element Simulation of Ti-6Al-4V Alloy with 3D Polycrystalline Models

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Abstract. Polycrystalline aggregate models are built based on the theory of Voronoi diagram, then crystal plasticity finite element method (CPFEM) is used to study the relationship of microstructures and stress-strain responses in Ti-6Al-4V alloy during uniaxial tensile tests at room temperature. Stress–strain responses of the Ti-6Al-4V alloy were investigated at different strain rate to study the deformation behavior. Based on the model, the effects of grain size, volume fraction of globular primary α_p -phase and strain rate on stress-strain responses are investigated. Results indicate that compared with strain rate and volume fraction of primary α_p -phase, grain size show a significant influence on stress-strain responses, the stress has a tendency of increase with the grain refinement. The strain distribution range of aggregates increases with increasing of the strain rate, the stress decreases with increasing of the volume fraction of primary α_p -phase.

Introduction

It's well known that titanium and its alloys are widely used as a key structural material in the aviation and space fields due to their superior strength to density ratio, excellent fatigue resistance and corrosion resistance, good biocompatibility and so on. Ti-6Al-4V is a common Ti-Al alloy possess excellent comprehensive performance, and used in a variety of structural engineering applications ranging from medical implants to compressor blades in gas turbine systems[1]. Because of its high strength over density ratio in the low to moderate range of service temperatures, Ti-6Al-4V principally used in the aerospace industry, such as fasteners and engine components[2]. It can be predicted that time dependent material behavior in the range of large strain rate by using material constitutive model. The constitutive law based on crystal plasticity theory can capture the information of both macro and micro deformation behaviors. So finite element simulation technology is a bridge of link the parameters of plastic deformation and the deformation process parameters, reduce the cost and provide production guidance. Taylor and Schmid et al did a lot of meaningful work in the early stages of the crystal plasticity theory development[3]. On the basis of their work, Hill and Rice made the mathematical description focus on Geometry and kinematics of crystal plastic deformation[4,5].

At present, an increasing number of researchers tend to study the deformation process by numerical approaches, such as the crystal plasticity finite element (CPFE) method[6-17]. The CPFE method can be used to predicting the microstructure-property relationships due to its special ability to acquire the details of microstructural features. The geometrical representations of grains is from simple to complex, rough to accurate[18-20]. The incompatibility of plastic deformation in a near β titanium alloy was analyzed based on the CPFE method[6], the results show that the plastic deformation in the two phases is incompatible, and the deformation behavior of α phase is significantly affected by the crystal orientation and loading direction. Chung-Hyun Goh et al[7] made a simulation of crystallographic plasticity in fretting of Ti-6Al-4V, results show that the

crystallographic orientation of the grains plays a significant role in the deformation response. Hamidreza Abdolvand et al[8] used Voronoi tessellation method and crystal plasticity finite element model studied stress heterogeneity within each individual grain of polycrystalline Zircaloy-2.

In the present work, a crystal plasticity finite-element model was developed for simulating the uniaxial tensile tests process at room temperature of Ti-6Al-4V alloy with 3D polycrystalline models. The grains was divided by Voronoi polyhedral by regular mesh. The influences of grain size, the volume fraction of primary α_p -phase and strain rate on stress-strain responses were investigated in this work.

Model description

Crystal Plasticity Theory

Deformation of the crystal can be decomposed into an elastic component and a plastic component. The former include both the elastic distortion and the rigid-body rotation, the latter contain the total deformation caused by crystallographic slip.

$$\mathbf{F} = \mathbf{F}^e \mathbf{F}^p. \quad (1)$$

where \mathbf{F}^e is both the elastic distortion due to lattice distortion and the crystal rigid-body rotation, and \mathbf{F}^p is the plastic deformation due to dislocation slip.

Similarly with multiplicative decomposition of deformation gradient, the velocity gradient is also decomposed a part with elastic distortion and the rigid-body rotation and a part with plastic deformation due to dislocation slip.

$$\mathbf{L} = \dot{\mathbf{F}}\mathbf{F}^{-1} = \dot{\mathbf{F}}^e(\mathbf{F}^e)^{-1} + \mathbf{F}^e\dot{\mathbf{F}}^p(\mathbf{F}^p)^{-1}(\mathbf{F}^e)^{-1}. \quad (2)$$

The plastic velocity gradient \mathbf{L}^p is

$$\mathbf{L}^p = \dot{\mathbf{F}}^p(\mathbf{F}^p)^{-1} = \sum_{\alpha} \dot{\gamma}^{\alpha} \mathbf{s}^{\alpha} \otimes \mathbf{m}^{\alpha}. \quad (3)$$

where $\dot{\gamma}^{\alpha}$ is the slipping rate.

The rate-dependent hardening equation is

$$\dot{\gamma}^{(\alpha)} = \dot{\gamma}_0^{(\alpha)} \left[\frac{\tau^{(\alpha)}}{g^{(\alpha)}} \right] \left[\left| \frac{\tau^{(\alpha)}}{g^{(\alpha)}} \right| \right]^{n-1} \quad (4)$$

where $\dot{\gamma}_0^{(\alpha)}$ is the reference shear strain rate, $g^{(\alpha)}$ is the reference shear stress, and n the rate sensitivity exponent of slip.

The strain hardening equation is

$$\dot{g}^{(\alpha)} = \sum_{\beta=1}^N h_{\alpha\beta} \left| \dot{\gamma}^{(\beta)} \right| \quad (5)$$

where $h_{\alpha\beta}$ is slip hardening moduli.

In 1982, Peirce made the crystal plasticity model numeralization successfully, whereafter Asaro and Needleman come up with the first rate dependent crystal plasticity constitutive relation and the corresponding numerical method. Peirce, Asaro and Needleman[21] proposed a simple form to describe the self-hardening modulus, called PAN model.

$$h_{\alpha\alpha} = h(\gamma) = h_0 \operatorname{sech}^2 \left(\frac{h_0 \gamma}{\tau_s - \tau_0} \right). \quad (6)$$

where h_0 represent the initial hardening modulus, τ_0 is the initial values of the critical resolved shear stress, τ_s is saturated flow stress.

Establishment of FE Model

In recent years, many studies have been focused on simulating polycrystal by using Voronoi diagram. A 3D Voronoi tessellation can be used to establish a model with stochastic grain shape, so more close to actual material structure. Basic conception of Voronoi diagram can be interpreted as a set of randomly distributed core influence zones in the space, and each polyhedron represents a grain. According to the metallographic structure obtained by experimental observation, the grain

size of Ti-6Al-4V alloy is 15 to 20 μm . Based on the theory of Voronoi diagram, polycrystalline aggregate models are built with different grain size in this work, grain size are 12 μm , 15 μm and 18 μm , respectively. A cubic model of scale of 0.07mm*0.07mm*0.07mm was built, the number of grain are 379, 194 and 112, respectively. Grain morphology is equiaxial, the duplex microstructure containing equiaxed primary α_p -phase and lamellar colony structure, the duplex microstructure discrete distribute randomly, the crystallographic orientations with similar probability density distributions are assigned to the finite element mesh. Fig.1 (a) (b) (c) shows the polycrystalline aggregate containing 112,194 and 379 grains.

On the basis of the model built above, Ti-6Al-4V alloy deformation process is simulated with uniaxial tensile tests at different strain rate by using Abaqus finite element simulation software. The boundary conditions of numerical tests are illustrated in Fig.2. Firstly, displacements of three adjacent surfaces of the polycrystalline aggregate are fixed. Then, displacement loading with constant strain rate is applied on the top surface along Y axis during calculation.

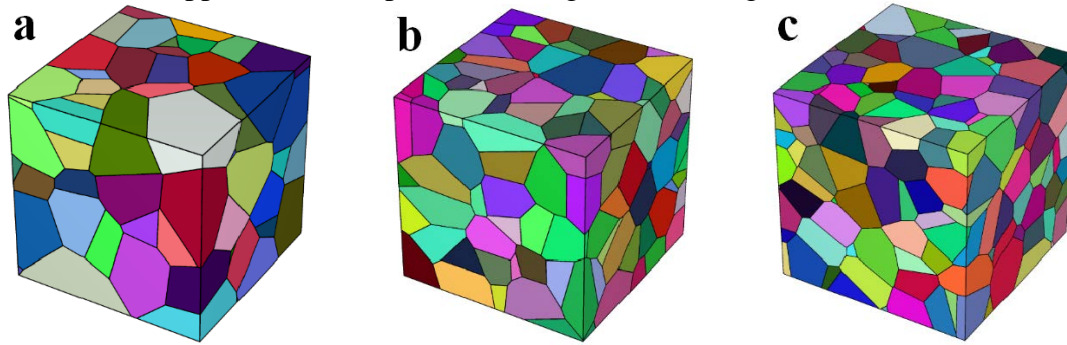


Fig.1 Polycrystalline aggregates with different grain size and boundary conditions of tensile tests.
(a) 18 μm . (b) 15 μm . (c) 12 μm .

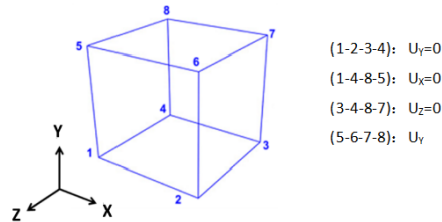


Fig.2 Boundary conditions of tensile tests.

Results and Discussion

The Material Parameters of the Ti-6Al-4V Alloy

Ti-6Al-4V alloy is a diphasic titanium alloy, so we need to get the material parameters of alpha and beta phase at room temperature. However, the volume of hexagonal close packed (hcp) α -phase is much more than body-centered cubic (bcc) β -phase, the volume fraction of the β phase is rather small. So, The structure of Ti-6Al-4V alloy used in the present model was a duplex microstructure containing globular primary α_p -phase nodules and the remaining is a lamellar structure of secondary α_s plates embedded in the β matrix[9]. The optical micrograph is shown in Fig.3. The elastic constants of Ti-6Al-4V alloy is $E=110,000$ MPa, poisson's ratio is $\mu=0.34$. The crystal plasticity parameters of three different slip systems, which are basal, prismatic and pyramidal, of equiaxed primary α grains are listed in Table 1. The point is that the reference shear rate, inverse strain rate sensitivity exponent and initial values of the yield strength of slip systems are obtained by fitting experimental data use trial-and-error method. The crystal plasticity parameters of lamellar structure in this work is increase in those grains by a factor of 1.25, e.g ($\alpha+\beta$ colonies)= 1.25(α_p nodulous) [9].

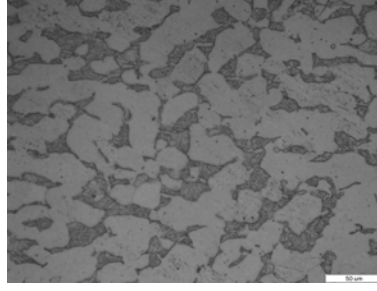


Fig. 3 Microstructure of the Ti-6Al-4V alloy.

Tab. 1 Crystal plasticity constants of Ti-6Al-4V.

Phase and slip system		$\dot{\gamma}_0$	n	h_0 (MPa)	τ_0 (MPa)	τ_s (MPa)
lamellar colony	Basal	0.001	50	11853	77.5	62.5
	Prismatic	0.001	50	11853	31.3	25
	Pyramidal	0.001	50	11853	65	52.5
primary α_p -phase	Basal	0.001	50	9482	62	50
	Prismatic	0.001	50	9482	25	20
	Pyramidal	0.001	50	9482	52	42

Effect of Grain Size on Stress-strain Response.

Effect of grain size on stress-strain response of aggregates are discussed in this section. The polycrystalline aggregates with grain size of 12 μm , 15 μm and 18 μm and dispersed with regular mesh contain 3375 elements, and simple uniaxial tensile tests are conducted. If no otherwise specified, 80 per cent of the volume fraction of globular primary α_p -phase, regular mesh with 3375 elements and strain rate of 0.001 s^{-1} are used. Results shown in Fig. 4. It indicates that the percentage of high stress area of the model increase with decreasing of the grain size. We can draw a conclusion that grain size has a significant influence on the overall stress. This is because the number of grain boundary increase with the grain refinement, the proportion of the grain boundary elements increased, stress concentration occurs in the grain boundary elements, which results to higher strength at grain boundary elements. Fig. 5 illustrates the stress-strain curve of aggregates with different grain size during uniaxial tensile tests when the overall strain is 0.1. It can be seen that the stress has a tendency of increase with the grain refinement. Simulation value is the mean of all integral points of aggregates, hereafter is the same.

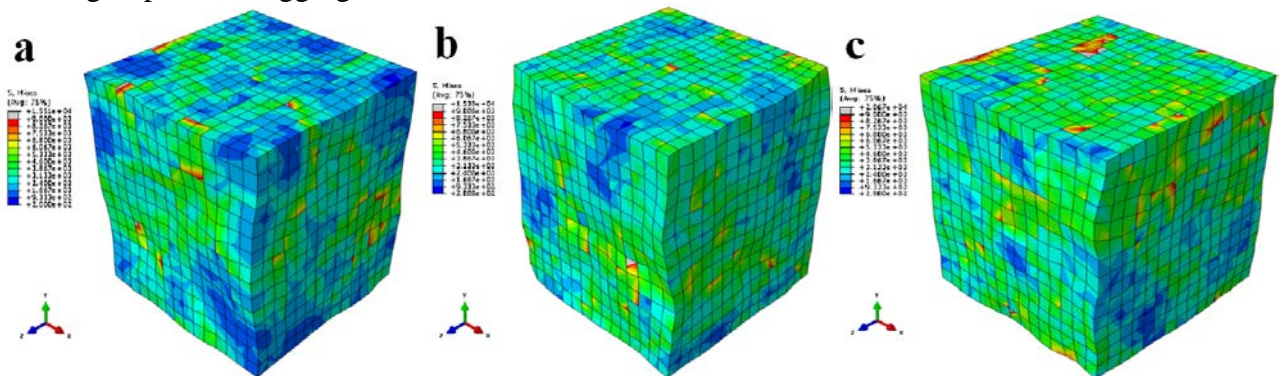


Fig. 4 Distributions of Von Mises equivalent stress of polycrystalline aggregates with different grain size when overall strain is 0.1. (a) 18 μm . (b) 15 μm . (c) 12 μm .

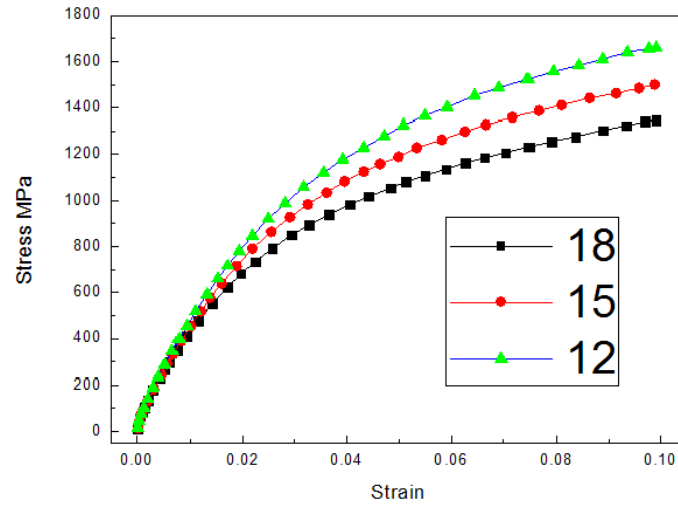


Fig. 5 Stress-strain curves of polycrystalline aggregates with different grain size.

Effect of Strain Rate on Stress-strain Response.

Fig. 6 illustrates the distributions of strain of aggregates comprised of 112 grains with 3375 hexahedron elements during uniaxial tensile tests when the overall strain is 0.1 and strain rate are 0.001 s^{-1} , 0.0002 s^{-1} and 0.00005 s^{-1} , respectively. From the strain nephogram, the overall strain increases with increasing of the strain rate, this is because force acts on the dislocation instantaneously in higher strain-rate condition, result in dislocation movement speed increase, many of the dislocation source start to move at the same time, besides, twins will appear at high strain rate. For these reasons, metallic materials shows additional hardening with increasing of the strain rate. Fig. 7 shows the stress-strain curve of aggregates calculated by Abaqus using 3375 hexahedron elements with different strain rate when the overall strain is 0.1. It is noted that strain rate has a slight influence on stress-strain responses.

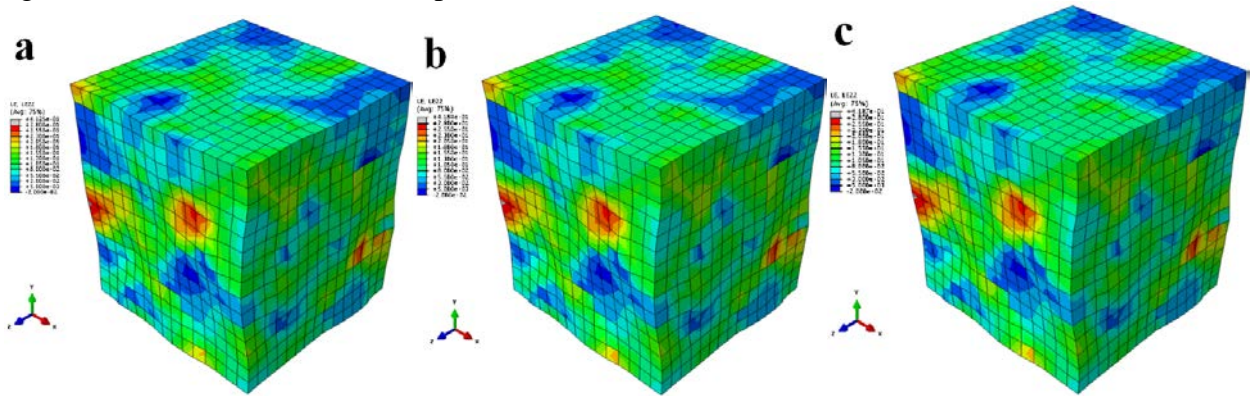


Fig. 6 Distributions of strain of polycrystalline aggregates with different strain rate when overall strain is 0.1. (a) 0.001 s^{-1} . (b) 0.0002 s^{-1} . (c) 0.00005 s^{-1} .

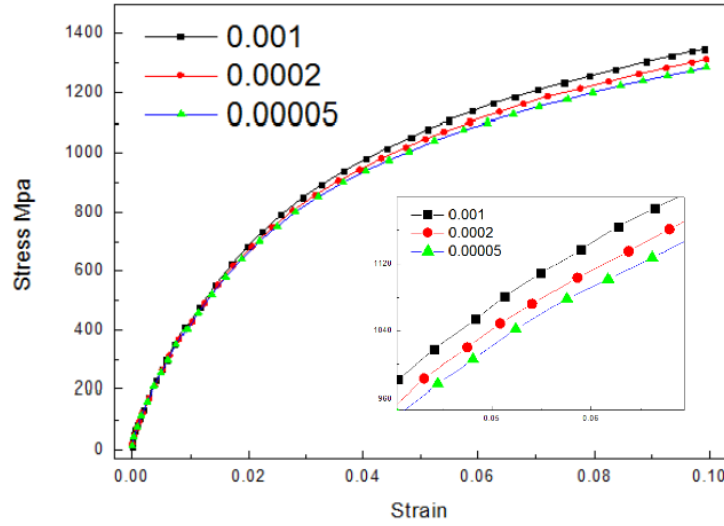


Fig. 7 Stress-strain curves of aggregates with different strain rate.

Effect of the Volume Fraction of Primary α_p -Phase on Stress-strain Response.

Fig. 8 presents the Von Mises equivalent stress distribution of aggregates with various volume fraction of primary α_p -phase when the overall strain is 0.1 and containing 112 grains with 3375 elements. The volume fraction of primary α_p -phase in this section are 20 per cent, 50 per cent and 80 per cent, respectively. From the Fig. 8, it can be seen that the Von Mises equivalent stress distribution range of aggregates decreases with increasing of the volume fraction of primary α_p -phase. The stress distribution of aggregates display primary α_p -phase only are shown in Fig. 9. Fig. 10 illustrates the stress-strain curve of aggregates containing 112 grains with different volume fraction of primary α_p -phase during uniaxial tensile tests when the overall strain is 0.1. The conclusion is that the stress decrease slightly with increasing of the primary α_p -phase.

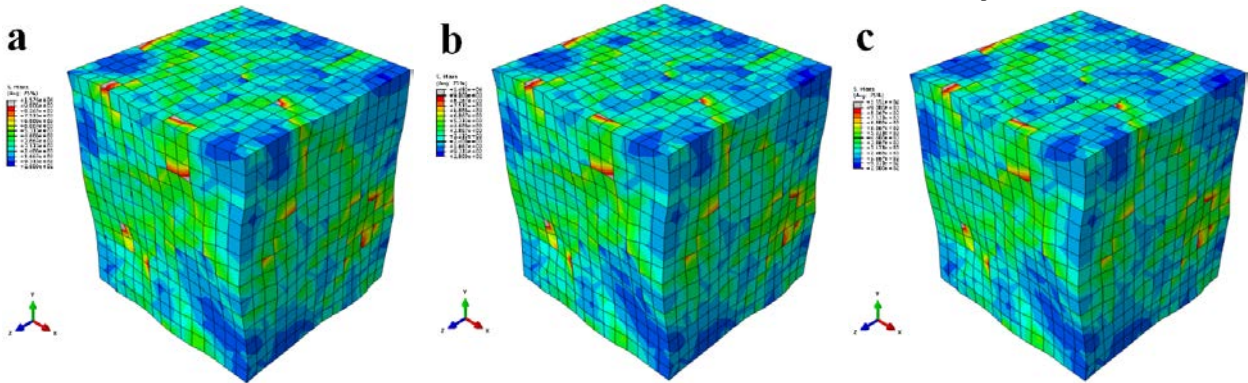


Fig. 8 Distributions of Von Mises equivalent stress of polycrystalline aggregates with different volume fraction of primary α_p -phase when overall strain is 0.1. (a) 20 %. (b) 50 %. (c) 80 %.

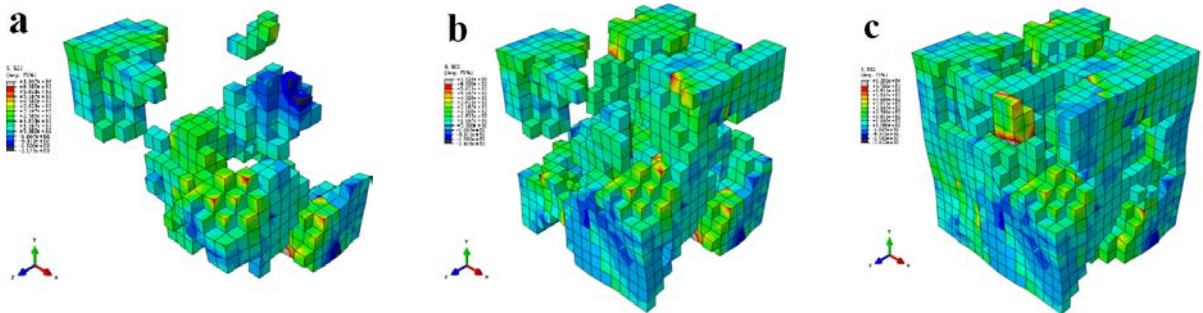


Fig. 9 Distributions of stress of aggregates display primary α_p -phase only with different volume fraction of primary α_p -phase when overall strain is 0.1. (a) 20 %. (b) 50 %. (c) 80 %.

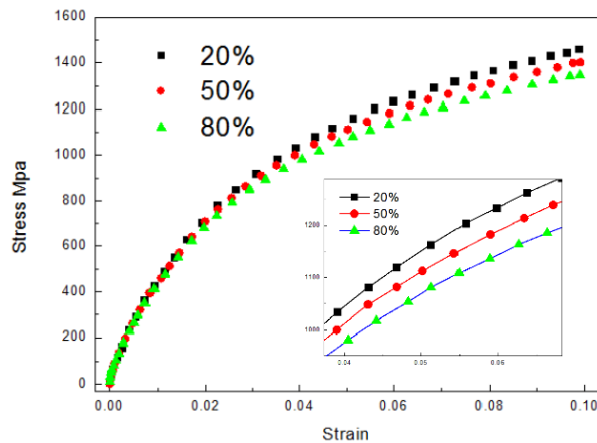


Fig. 10 Stress-strain curves of aggregates with different volume fraction of primary α_p -phase.

Conclusions

- 1) Based on crystal plasticity finite element simulations, the polycrystalline aggregate models are established by means of Voronoi diagram method in this work. The uniaxial tensile tests process of the Ti-6Al-4V alloy under the condition of constant strain rate was studied. The regular mesh are used to disperse the models. The parameters of the Ti-6Al-4V alloy are got by trial-and-error method.
- 2) This paper investigated the effects of grain size, the volume fraction of primary α_p -phase and strain rate on stress-strain responses.
- 3) Results show that strain rate has a slight influence on stress-strain responses, whereas the grain size show a significant influence on stress-strain responses. Stress concentration occurs in grain boundaries due to the discontinuity of orientation, the percentage of high stress area increase with grain refinement. The higher strain rate, the higher stress of the polycrystalline aggregate. The stress decreases with increasing of the primary α_p -phase.
- 4) We can see some deficiencies in the model. For example, more perfect grain boundary model still need to build, not considering complication of the material deformation mechanism, such as twin deformation mechanism. In addition, the superplastic deformation mechanism under high temperature still need to further study. The improved model can provides enhanced understanding of the plastic deformation, especially with regard to the superplastic deformation process.

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