

Analysis of the Dynamic Characteristics of Seat Headrest During Impact

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Abstract. A energy-absorber device with gravity pendulum of car seat headrest is introduced in this paper, and has a analysis at the dynamic characteristics of headrest by use the method of three component-force detection. A force measuring system from the three component-force detection is brought up to reseach the model error in impact model, and obtained the point, which the model has a minimum error. Finally, the impact model was simulated with MATLAB by computer, as a results show that the simulattion curves are similar to the real response curves very much.

Introduction

Due to the important of safety and convenience, car seats become an object of study with the advent of the car in automakers. In collision accident, whiplash is one of the major damage for occupant. Thanks to the emergence of the car seat headrest, the economic and casualties caused by traffic accident has greatly reduced. The principle of reduce damage could describe as by impose restrictions on occupant head, the relative displacement between the head and body is limited, it ensures the reduction of the whiplash. Therefore, as a key part of automobile seat, the technical requirements for seat headrest is the most severe in required and a lot of experiments is necessary, before headrest leaving the factory^[1]. Because of the dynamic performance of the seat headrest during impact, is affect on seat safety directly, energy absorbed properties became one of the most important bases for evaluating the quality of seat headrest. In this paper, a second order control model is established to analysis the dynamic performance of the headrest, lay the foundation for follow-up study by confirm the appropriate parameters in simulation.

The Basic Structure and Principle

The device of impact testing. The device of seat headrest impact testing can be classified in two types according to impact energy access: on the basis of ejection, a power soure with hydraulic or pneumatic was carried out on the headrest^[2,3]; on the basis of potential energy transduction principle, provide the impact energy by gravity pendulum^[4,5]. However, each one of these prime mover are aim to get an instantaneous impact at seat headrest, in this paper, pendulum impact testing machine is the object of research platform.

Among mang detection techniques of dynamic characteristics of the seat headrest, because of the structure of the headrest, the different position, and the uncertainty of the impact point, the impact force become difficulties in testing^[6]. The method, which called three component-force detection, is commonly used in single point impact detect, is introduced as the basic analysis theory of the headrest^[7].

As it is shown in figure 1, typically, an energy absorbing machine of automobile seats, which mainly consists of angle sensor, pendulum pole, head model, motor, seats, support and the foundation. In actual work, by the driving of the motor swing rod turning an angle, and make the pendulum to rise a certain height, gravitational potential energy will transforms into impact energy, when motor released, to complete the absorption test of the seat^[8].

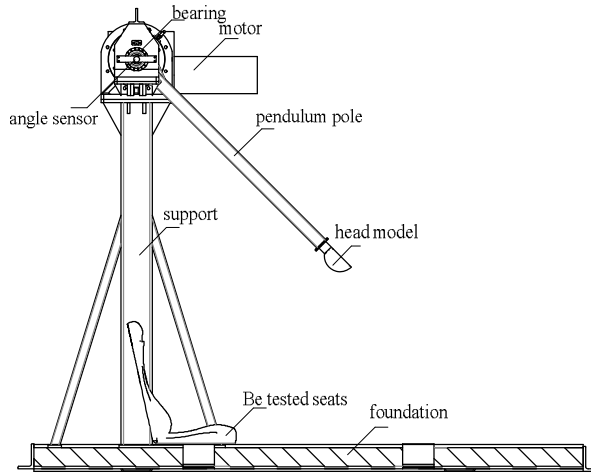


Fig. 1 Structure of energy absorbing machine

Model of impact testing. The method of three component-force detection, in order to reduce the error caused by impact of uncertainty, there are three pressure sensor evenly place in a plane with 120° . Take the interface between the headrest and pendulum as a zero thickness and weight circular plate, and take the headrest as a mass spring damping system, establishes a mathematical model as it is shown in figure 2.

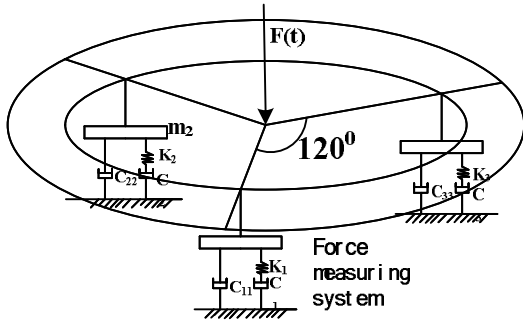


Fig. 2 The model of three component-force detection

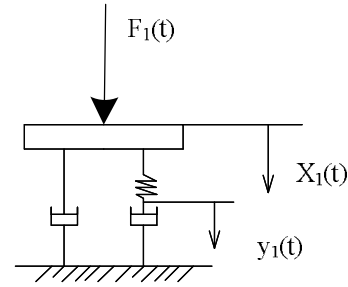


Fig. 3 Force measuring system

In Fig.2, $F(t)$ is the impact in seat headrest, k_1, k_2, k_3 is three pring stiffness and $C_1, C_{11}, C_2, C_{22}, C_3, C_{33}$ is the six damping coefficient in each fore measuring system. For comparison, as shown Fig.3, a monomer force measuring system was selected as a study subjects, $F_1(t)$ is one of the force, impacting in headrest, and $X_1(t), y_1(t)$ is the displacement of seat headrest and spring. According to the theory of dynamics, we can reach $F(t) = F_1(t) + F_2(t) + F_3(t)$.

For the force measuring system, has an equation of state:

$$\begin{cases} k_1[x_1(t) - y_1(t)] = cy_1'(t) \\ F_1(t) = m_1x_1''(t) + cx_1'(t) + k_1[x_1(t) - y_1(t)] \end{cases} \quad (1)$$

With simplified and Laplace transform, the relationship between input impact and output displacement can be drawn from Eq. 1:

$$G_1(s) = \frac{F_1(t)}{X_1(t)} = \frac{c_1s + k_1}{m_1c_1s^3 + (k_1m_1 + c_1^2)s^2 + 2c_1k_1s} \quad (2)$$

Without losing generality, Eq. 2 could be describe as

$$G_1(s) = \frac{s + z_1}{s(s^2 + 2\zeta w_{n1} + w_{n1}^2)} \quad (3)$$

Where , the natural frequencies was derived by $w_{n2} = \sqrt{\frac{k_2}{m_2}}$, and damping ratio was derived by $x_1 = \frac{c_1}{\sqrt{m_1 k_1}} + \frac{\sqrt{m_1 k_1}}{c_1}$, and there has a position of zero in $z = \frac{k_1}{c_1}$.

The same force measuring system 2 and 3 may be easily adapted to obtain:

$$\begin{cases} G_2(s) = \frac{s + z_2}{s(s^2 + 2xw_{n2} + w_{n2}^2)} \\ G_3(s) = \frac{s + z_2}{s(s^2 + 2xw_{n3} + w_{n3}^2)} \end{cases} \quad (4)$$

Where, as the same to the force measuring system1, there natural frequencies and damping ratio were derived by:

$$\begin{cases} w_{n2} = \sqrt{\frac{k_2}{m_2}} & w_{n3} = \sqrt{\frac{k_3}{m_3}} \\ x_2 = \frac{c_2}{\sqrt{m_2 k_2}} + \frac{\sqrt{m_2 k_2}}{c_2} & x_3 = \frac{c_3}{\sqrt{m_3 k_3}} + \frac{\sqrt{m_3 k_3}}{c_3} \end{cases} \quad (5)$$

And, their position of zero is $z_2 = \frac{k_2}{c_2}$ and $z_3 = \frac{k_3}{c_3}$.

The model analysis

The error analysis of the model. From the point of detection, the impacting in headrest is a transient signal, and the exciting source is a pulse signal. Simplified, assuming input function to be impules, we can reach the response function of the force measuring systems as: $X_{on}(s) = G_n(s)X(s)$, $n=1,2,3$, and there has $X_i = L[d(t)] = 1$, $X_{on}(s) = G_n(s)$, therefore, could obtain a further decomposed as shown in Eq.6 for response function:

$$X_{oi} = \frac{A_i}{s} + \frac{B_i s + C_i}{s^2 + 2x_i w_{ni} + w_{ni}^2}, i=1,2,3 \quad (6)$$

Where, $A_i = 1$; $B_i = -1$; $C_i = 2x_i w_{ni} - 1$ are constant determined by partial fraction. Further, as it described in Eq. 7, the unit pulse response of force measuring system is derived by using the inverse Laplace transform from Eq. 6:

$$x_n(t) = A_i + \sqrt{1 + \left(\frac{3x_i w_{ni} - 1}{w_{ni}}\right)^2} \exp(-x_i w_{ni} t) \sin[w_{ni} t + \arctan\left(\frac{w_{ni}}{1 - x_i w_{ni}}\right)] \quad (7)$$

As it known, the three force measuring system in model of seat headrest impact test, has the same model features. So that, take one of their as the measurement reference, while, the displacement errors of the detection system, caused by the uncertainty of the impact point and the inhomogeneity of dynamic characteristics between pressure sensor and the plate, have been obtained:

$$e = \frac{x_i(t) - x_1(t)}{x_1(t)}, i=2,3 \quad (8)$$

To obtain the peak error of the model, take the derivative of the Eq. 7, reach the peak value as it shown in Eq. 9:

$$x_n(t_{\max}) = A_i + \sqrt{1 + \left(\frac{3x_i w_{ni} - 1}{w_{ni}}\right)^2} \exp\{-x_i \times [\arctan(\frac{1}{x_i}) - \arctan(\frac{w_{ni}}{1 - x_i w_{ni}})]\} \sin(\arctan \frac{1}{x_i}) \quad (9)$$

Take other two force measuring system into the displacement error consider, the displacement error between the force measuring system 1 and force measuring system 2 can be obtained by substituting response function of force measuring system 2 into the Eq. 8:

$$e = \frac{\sqrt{1 + x_1^2} \exp[x_1 \arctan(\frac{1}{x_1}) + \arctan(\frac{w_1}{x_1 w_1 - 1})] * \sqrt{\left(\frac{3w_2 x_2 - 1}{w_2}\right)^2 + 1}}{\sqrt{1 + x_2^2} \exp[x_2 \arctan(\frac{1}{x_2}) + \arctan(\frac{w_2}{x_2 w_2 - 1})] * \sqrt{\left(\frac{3w_1 x_1 - 1}{w_1}\right)^2 + 1}} - 1 \quad (10)$$

According the Eq. 10, it can be deduced that, if the force measuring systems are statistical consistency, the error e can be eliminated, but in the practical engineering, the errors always exist, and we can determine the parameters through choosing the right error values.

The simulation of the model. For conform with the actual situation, define $a = x_n / w_n$, $n = 1, 2, 3$ as a proportional between the natural frequencies and damping ratio. Assuming that, a has a respective value at 1%, 2% and 3%. According to Eq. 10, the relationship between the e and x can be obtained, as shown in Fig. 4. It can be concluded that, the increase of error coefficient with the increase of the damping coefficient, however, the error has the same values at the point where $x = 1$. This means, in the system of model, there is a minimum error at this point.

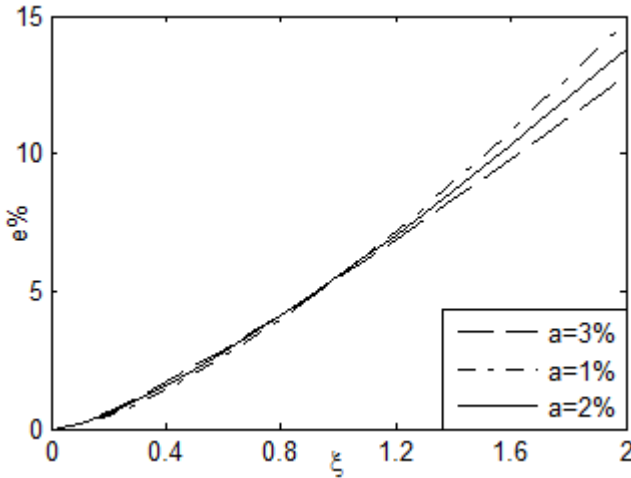


Fig. 4 Relationship between the e and ξ

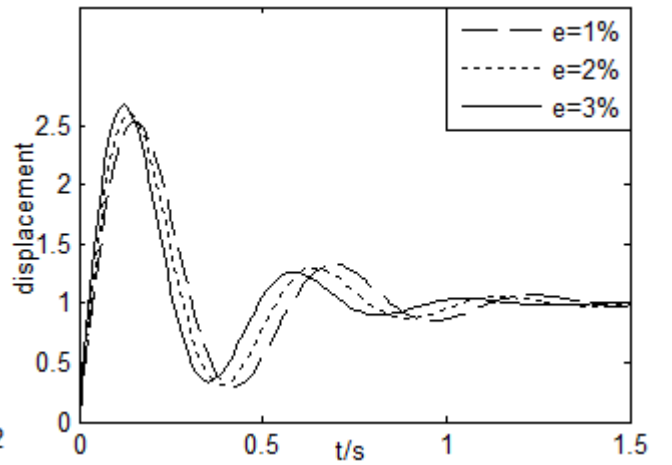


Fig. 5 Simulation of the model

Therefore, take the model into MATLAB for simulation with the assumption that the damping ratio a has values at 1. Although the natural frequencies have no effect on error, the time-domain response of the force measuring system is affected by natural frequencies, as can be seen from Eq. 9, as a result, assuming the natural frequencies is 10. And for conform with the actual situation, we also assume the error with the percentage at 1%, 2% and 3% exists, the results of simulation are shown in Fig. 6.

According to Fig. 6, the model has different peak amplitudes caused by error, and the time about peak amplitude is also affected by error. And contrast with the actual testing, which discusses in literature [9], the model is well conform with the actual situation.

Conclusion

This paper researches the dynamic characteristics of seat headrest during impact by analyzing the model of the impact testing. A method of three component-force detection is established in the paper and the characteristics of the force measuring system have been analyzed; the analysis of the model error

is researched much further. At the same time, the relationship between the damping ratio and error is been obtained. Finally, the impact model was simulated with MATLAB by computer, it is obvious that the curves are similar to the real response curves very much.

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