Dislocation multiplication behavior of AZ61 magnesium alloy during cyclic bending

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Abstract. The dislocation multiplication behavior of AZ61 magnesium alloy during cyclic bending vibration was investigated. The results show that with the increase of strain amplitude and shear stress, the process of dislocation multiplication behavior contains dislocation slipping, dislocation multiplication and dislocation extension, and dislocation multiplication phenomenon accords with Frank–Read source mechanism. At last, the mobility dislocation number and the dislocation density in AZ61 magnesium alloy increase significantly with the increase of strain amplitude.

Introduction

Magnesium alloy is the lightest structural material with excellent damping capacity. The result shows that the dislocation movement and the change of mobility dislocation density (Dislocation length per unit volume) in magnesium alloys significantly affect dislocation damping capacity at room temperature [1-5]. And, further researching on the micro-theory of metal mechanical properties, it shows that dislocation multiplication caused by shear stress is responsible for dislocation movement and the change of mobility dislocation density [6]. Therefore, the process of dislocation multiplication behavior and the change of mobility dislocation density caused by dislocation multiplication are important foundations of researching on the dislocation damping mechanism of magnesium alloys. However, up until recently, very little attention has been paid to study the process of dislocation multiplication in magnesium alloys.

Cite the mechanics of materials as a reference, we can see the shear stress generates in the rectangular beam when the beam is in condition of cyclic bending vibration. This study takes cyclic bending vibration mode of the rectangular beam as the research object, and the aim of this study is to study the process of dislocation multiplication in AZ61 magnesium alloy as the strain amplitude increase.

Experimental procedures

Magnesium alloy preparation

Commercial cast AZ61 magnesium alloy (5.5-7.0 wt%Al, 0.5-1.5 wt%Zn, 0.15-0.5 wt%Mn) was used as the material.
Treatment on magnesium alloy rectangular beam

AZ61 magnesium alloy rectangular beam was cut via wire electrical discharge machining. The dimension of the magnesium alloy rectangular beam was 500 mm×15 mm×7 mm. Then, the rectangular beam was treated via cyclic bending deformation, loaded in the middle of beam length, which is shown in Fig. 1. The loading parameters are shown in Table 1.

Table 1 Loading parameters of the beam

<table>
<thead>
<tr>
<th>strain amplitude</th>
<th>bending cycle</th>
<th>frequency</th>
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<td>5×10^{-3}</td>
<td>100</td>
<td>2Hz</td>
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</table>

Direction & distribution of shear stress in the beam

When the beams were in condition of cyclic bending vibration, the direction & distribution of shear stress in the beam was studied. The dimensions of the rectangular beam (a₁=500mm, b₁=15mm, c₁=7mm) are shown in Fig. 1.

![Fig. 1. Dimensions of the rectangular beam and direction & distribution of shear stress](image)

S₁ is the shear stress action face; S₂ is the parallel layer with the neutral layer

The direction & distribution of shear stress τ in S₁ layer is shown in Fig. 1 and formula (3)

\[
\tau = \frac{F \sin(\omega t) (b_1^2 / 4 - y^2)}{4 I_\varepsilon}
\]

(1)

\[
\varepsilon = \frac{\sigma}{E} = \frac{F \sin(\omega t) a_1 b_1}{8 I_\varepsilon E}
\]

(2)

\[
\tau = \frac{2(b_1^2 / 4 - y^2)E}{a_1 b_1} \varepsilon
\]

(3)

Where, τ is the shear stress value in S₂ layer, ε is strain amplitude, y is the distance of the parallel layer to the neutral layer, Fsin(ωt) is the load, I_ε is inertia moment, E is elastic modular.

Preparation of transmission electron microscope (TEM) observation sample

It was calculated that direction of the shear stress inside the bent beam is identical to the load, so a slice (6 mm×6 mm×0.5 mm) was cut via wire electrical discharge machining at the position in the shear stress action face, it is shown in Fig. 2, the point O is the center of the sample.
The shear stress value in neutral layer is the largest in the rectangular bending beam, calculation of the largest shear stress at point O is as follows.

$$\tau_{\text{max}} = \frac{E b_1}{2a_1} \varepsilon$$  \hspace{1cm} (4)

Finally, TEM foil was prepared by ion-thinning after mechanical grinding from the slice sample. The diameter of the TEM foil is 3 mm, the Point O in Fig. 2 is the center of the TEM foil. The observation area was around the point O.

**Results and discussion**

**Observation of dislocation**

The dislocation images were observed by TEM. Fig. 3 shows that dislocation source has been slipped and multiplied, it has formed many dislocation loops. In Fig. 3a and Fig. 3b, it can be seen that the dislocations multiplied and extended uniformly, specifically, many dislocation loops in a hemicycle multiplied and extended uniformly in Fig. 3b. The result is the dislocation density increases obviously when the beam was been cyclic bending.

![Fig. 3 The images of dislocation slipping and multiplication](image)

Form the above dislocation images, it can be found that the dislocation multiplication behavior has taken place, and the dislocation multiplication accords with F-R source mechanism. The process of dislocation multiplication caused by shear stress is shown in Fig. 4. The result is the dislocation number and the dislocation density in AZ61 magnesium alloy increase significantly with the increase of stain amplitude.
Conclusions

Summarizing the detailed research that we have carried out on the dislocation multiplication behavior of AZ61 magnesium alloy in condition of cyclic bending vibration, we could come to the following conclusions:

1. The dislocation multiplication caused by the shear stress accords with Frank–Read source mechanism.
2. The process of dislocation multiplication behavior contains dislocation slipping, dislocation multiplication and dislocation extension.
3. The mobility dislocation number and the mobility dislocation density in AZ61 magnesium alloy increase significantly with the increase of stain amplitude.

The results are important foundations of researching on the dislocation damping mechanism and the change of mechanical properties of magnesium alloys.

Acknowledgments

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References


