Study on evaluation method of dynamic performance of generator

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Abstract. The stability of power system is affected by the dynamic performance of generator. This paper describes a evaluation method of dynamic performance of generator and the establishes the model of dynamic simulation in BPA, which proves that the method is practical and effective by compared with the actual test curve.

Introduction

With the rapid expansion of ultra high voltage grid, power system of China realizes the leap frog development. Analysis and simulation will provide a powerful technical support for the power system. The model parameters of generator, excitation system, governor and load are important for dynamic simulation of power system, the accuracy of which will directly affect the results of simulation. This paper focuses on the evaluation method of dynamic performance of generator.

The introduction of governor system

The role of turbine governor system can make the output power equal to the load, which has significant effect on dynamic stability and long-term stability of power system. Using the different model and parameters of turbine governor system in stability calculation of power system, the results of simulation will have a greater difference. The typical model of turbine governor system is shown in figure 1.

![Fig.1 The typical model of turbine governor system](image)

The evaluation indicators of dynamic performance of generator

The actions of the governor system will be recorded when the system disturbance occurs, which can be used to evaluate the dynamic performance of governor. The load adjustment will take sometime, which is caused by action of Primary frequency, therefore the dynamic performance of governor needs to be evaluated when the load is stable.
The speed deviation is:
\[ \Delta n' = \frac{\Delta n}{3000} \]  
(1)

Per-unit value of regulating pressure is:
\[ P_{1e} = P_{io} \times \frac{P_S}{N_o} \]  
(2)

Per-unit value of the deviation of regulating pressure is:
\[ \Delta P' = \frac{\Delta P_i}{P_{1e}} \]  
(3)

Per-unit value of load deviation is:
\[ \Delta N' = \frac{\Delta N}{P_o} \]  
(4)

Speed fluctuation rate (Considering pressure) is:
\[ \delta' = \frac{\Delta n'}{\Delta P_i} \]  
(5)

Speed fluctuation rate (Considering load) is:
\[ \delta' = \frac{\Delta n'}{\Delta N'} \]  
(6)

Frequency variation is:
\[ f_{MAX} = \text{Max}(f), (\text{EffetTime} < i < \text{UneffectTime}) \]  
(7)

Active power before the disturbance is:
\[ N_p = \frac{f_s}{2} \sum_{i=a}^{b} N_i, (a = \text{StartTime} - \frac{2}{f_s}, b = \text{StartTime} - 1) \]  
(8)

The example of verification
This paper establishes one machine-infinite bus system in the simulation system of BPA, which is shown in figure 2.

Fig.2 the one machine-infinite bus system

The model of turbine governor system established in this paper adopts experimental data, using the actual frequency difference in experiment as the input. The dynamic performance of turbine governor system can be evaluated by comparing the result of simulation and experiment. The comparison of simulation frequency difference with experimental frequency difference is shown in figure 3.
The step-up comparison of simulation active power with experimental active power in CCS power control mode is shown in figure 4.

The step-down comparison of simulation active power with experimental active power in CCS power control mode is shown in figure 5.

Conclusions

This paper establishes one machine-infinite bus system in the simulation system of BPA, using the experimental parameters of turbine governor system to simulate, and comparing the simulation results with the field test results. The study of this paper shows that the simulation curves are more fit to experimental curves, which illustrate the evaluation method proposed in this paper is practical and effective.

References


