

Design and Analysis in Multiple-Scissor-Linkage Applied to the Robotics Arm

Nan Hua^{1, 2, a}, Zhangong Xie^{1, b*}, Liangwei Luo^{1, 2}, Xianshuai Chen¹, David J. Tang³, Hong Zhang²

¹Guangzhou Institute of Advanced Technology, Chinese Academy of Sciences, Guangdong, China

²Guangdong University of Technology, 100 Waihuanxi Drive, China

³Smart Line Systems Inc., U.S.A.

^anan.hua@gjat.ac.cn, ^bzg.xie@gjat.ac.cn

Keywords: MSL, scissor linkages, modularity, extending length, precise movement, robotics arm
Abstract. Multiple-Scissor-Linkage (MSL) is kinematic mechanic, and to be a means for using two or more pairs of scissor linkages operating in different planes for moving a device in linear or nonlinear motions specifically. It is a modular component that constructs long extending, high precise movement and stronger robotic arms. It should reach much longer distance than conventional joint robotic arm because the multiply bar linkages like multiply arms connected one end to another.

Introduction

Robotics arm is the most welcome application in the field of robotic technology which is adopted in automation machinery equipment, military, industrial manufacturing, entertainment services, and exploration, universally, and other fields can be seen [1]. However, most of the robotics arms have limited workspace of the motion, large volume and heavy weight, sophisticated control system and so on. It intends to design the MSL to replace the upper and lower arms of conventional robots in this paper.

The MSL arm is made of aluminum alloy, so the weight is further reduced without affecting the mechanical performance. At the same time, by omitting an R-V reducer which is mounted on the joint between the upper arm and the lower arm, and mounting one motor to the base plate, this novel robotics arm reduces the cost and the inertia which is generated during the operation. Furthermore, MSL arm has easier and more precise method than the conventional robotics arm when controlling the motion.

MSLs have abroad applications in many fields such as aviation, construction and traffic transport, et al. and drawn the attention of scholars both at home and abroad. K. K. Vu etc. proposed a new kind of deployable tension-strut structure, which is composed of a plurality of units made of bars and tether [2]. C. Gante etc. proposed a curved deployable space frame [3,4]. The new MSLs, composed of multiple scissor units' parallel, are spherical. On the foundation of this research, Jian S. Dai designed a complex structured ball based on mechanism decomposition and equivalent screw system analysis [5].

Designation of the quadrangular MSL arm

Structural designation of the quadrangular MSL. Planar MSL will perform satisfactorily mechanical properties when receiving the effection from the vertical force. However, it's bending strength is greatly weakened when receiving the effection from the side force. The larger extending length the planar MSL reach, the weaker the bending strength performs. Therefore, to take full advantage of the planar MSL and fully avoid its disadvantaged, this paper adopts quadrangular MSL. The quadrangular MSL can bear side force and inertial force simultaneously. Each link is connected to other links by the pin to form a planar MSL as shown in Fig.1, and four planar MSLs form a quadrangular MSL by the middle of the connection device as shown in Fig.2. In order to meet the requirements of rapid response during the movement, each pin groove are used ball bearings (It mainly

bears radial force, and it can bear axial force, and its friction coefficient is 0.0010~0.0015) to support itself and transfer movement.

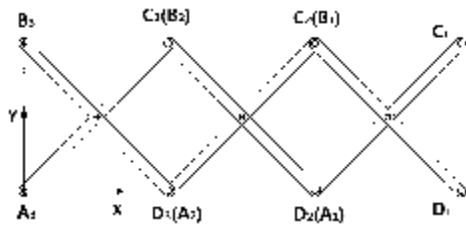


Fig.1. Planar MSL's Structure

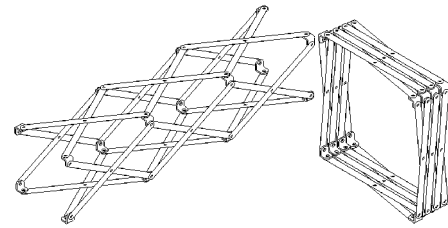


Fig.2. Quadrangular MSL's Structure

The joint of the MSL arm. There are two schemes about quadrangular MSL's transmission shown in Fig.3. Scheme one is that the mortar is mounted in point D. That means the point D is fixed, while the point A, B and C are moved to the point D. Scheme two is that the mortar is mounted in the quadrilateral middle position. This paper decides to choose the scheme one, because it can offer larger dimension's space, and it can be easier on position control.

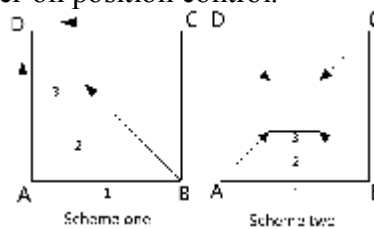


Fig.3. Transmission schemes of quadrangular MSL

In order to meet the requirements of rapid response, well vertical force performance and well side force performance, this paper adopts the linear module which is composed by ball screws and linear guide to achieve these transmission above. This paper also use 45 ° bevel gear to transmit the servo motor power to the linear module. But we should know how to select them.

As shown in Fig.4, if we apply the external forces (F_C and F_D) in the point C and point D, then we can solve the constraint forces (F_A and F_B) in the point A and point B.

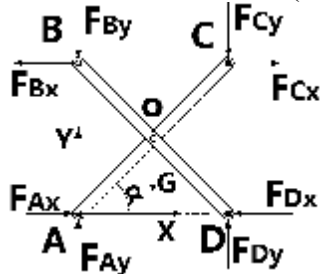


Fig.4. MSL unit's mechanical analysis

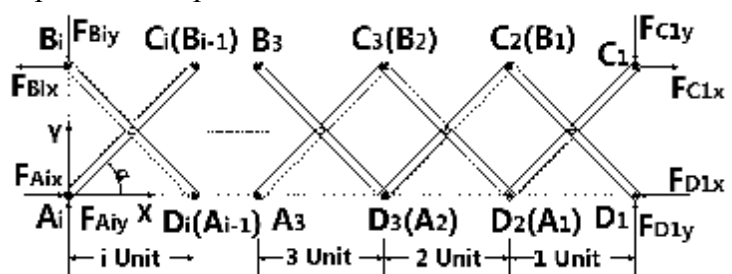


Fig.5. Planar MSL's mechanical analysis

This paper establishes the following equations based on force / torque equilibrium conditions:

$$\begin{bmatrix} F_{Dy} - F_{Cy} - G/2 & F_{Bx} - F_{Cx} & 0 \\ F_{Dy} - F_{Cy} - G/2 & F_{Ax} - F_{Dx} & 0 \\ F_{By} - F_{Cy} & F_{Bx} - F_{Cx} & 0 \\ 0 & 0 & F_{Ay} + F_{Dy} - G - F_{By} - F_{Cy} \end{bmatrix} \begin{bmatrix} \cos a \\ \sin a \\ 1 \end{bmatrix} = 0 \quad (1)$$

Where, G is one weight concerning the MSL unit. Solutions of these equations get:

$$F_A = \begin{bmatrix} F_{Ax} \\ F_{Ay} \end{bmatrix} = \begin{bmatrix} (G/2 + F_{Cy} - F_{Dy}) \cdot \cot a + F_{Dx} \\ F_{Cy} + G/2 \end{bmatrix} \quad (2)$$

$$F_B = \begin{bmatrix} F_{Bx} \\ F_{By} \end{bmatrix} = \begin{bmatrix} (G/2 + F_{Cy} - F_{Dy}) \cdot \cot a + F_{Cx} \\ F_{Dy} - G/2 \end{bmatrix}$$

Based on it, it will solve planar MSL's constraint forces (F_{Ai} and F_{Bi}) of the i unit. As shown in Fig.5, if we apply the external forces (F_{C1} and F_{D1}) in the point C_1 and point D_1 , then we can solve the constraint forces (F_{A1} and F_{B1}) in the point A_1 and point B_1 ,

As i is a odd number, that

$$F_{Ai} = \begin{bmatrix} F_{Aix} \\ F_{Aiy} \end{bmatrix} = \begin{bmatrix} (iG/2 + F_{C1y} - F_{D1y}) \cdot \cot \alpha + F_{D1x} \\ F_{C1y} + iG/2 \end{bmatrix} \quad (3)$$

$$F_{Bi} = \begin{bmatrix} F_{Bix} \\ F_{Biy} \end{bmatrix} = \begin{bmatrix} (iG/2 + F_{C1y} - F_{D1y}) \cdot \cot \alpha + F_{C1x} \\ F_{D1y} - iG/2 \end{bmatrix}$$

When i is even number, that

$$F_{Ai} = \begin{bmatrix} F_{Aix} \\ F_{Aiy} \end{bmatrix} = \begin{bmatrix} (iG \cdot \cot \alpha) / 2 - F_{D1x} \\ iG/2 - F_{D1y} \end{bmatrix} \quad (4)$$

$$F_{Bi} = \begin{bmatrix} F_{Bix} \\ F_{Biy} \end{bmatrix} = \begin{bmatrix} (iG \cdot \cot \alpha) / 2 - F_{C1x} \\ -F_{C1y} - iG/2 \end{bmatrix}$$

Simulation and analysis. As we know above, if α is 20° ($20^\circ \leq \alpha \leq 85^\circ$), the MSL arm will be in a critical state. So this paper decides to establish the simulation and analysis for the quadrangular MSL and planar MSL as the α is 20° . The results of equivalent stress for quadrangular MSL are shown as Fig.6. The maximum stress value is about 51.432Mpa which is far less than the AL7075's allowable stress ($[\sigma] = \sigma_s / n_s = 505 / 1.3 = 388.462$ Mpa). That means the mechanical formance is satisfactory. Then, when we establish the modal simulation and analysis, we can get results and make comparison of quadrangular MSL and planar MSL as the Fig.7 shown. When the order is one, the natural frequency of planar MSL is 1.503Hz. However, the natural frequency of planar MSL is 9.100Hz which is nearly nine times of the planar MSL. The MSL should keep away from the natural frequency above avoiding substantial structural vibration during the launched or folding process.

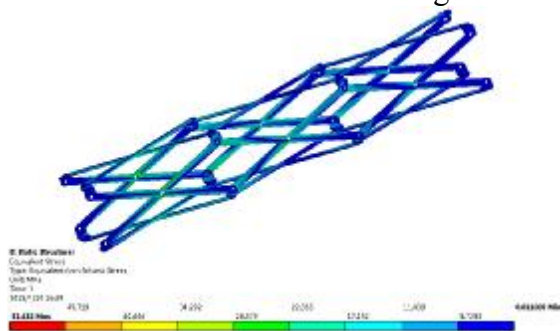


Fig.6. Stress analysis of quadrangular MSL

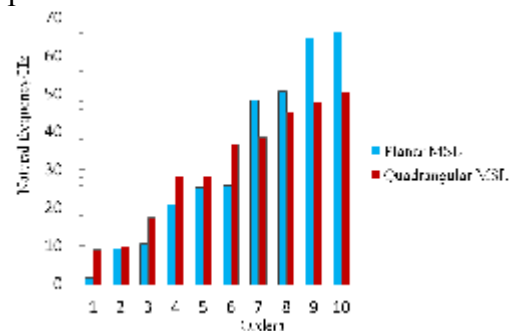


Fig.7. Comparison of modal analysis

Position Control of the Arm and a Prototype

Based on the theoretical analysis above, we can get the basic structure of the quadrangular MSL arm which is shown as the Fig.8. The Fig.8 shows that the quadrangular MSL has been extended to the furthest position. Then this paper will discuss how to drive the prototype to reach the destination precisely in the way we require.

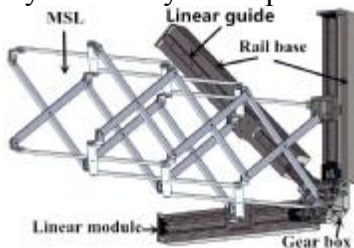


Fig.8 The prototype of the arm

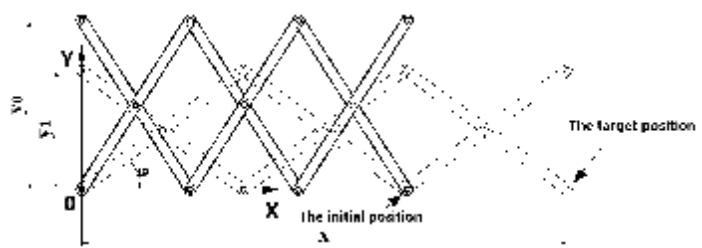


Fig. 9 The position control of the arm

As shown in Fig.9, we can get the following approximate geometrical relationship,

$$x = n \cdot l \cdot \cos \alpha \quad (5)$$

Where, x is the position of the target position of the arm, l is the length of the bar, α is the degree between bars and centerline of the arm, and n is the number of the MSL units.

Then we can obtain the relationship between the position of X direction and that of Y direction,

$$y_1 = (x \cdot \tan \alpha) / n \quad (6)$$

Where, y_1 is the length sensing on base by linear transducer.

As shown in Fig.8, the driving part of the arm is composed of servo motor and lead screw, which widely used in today's Computer Numeric Control (CNC) of machine tools. Lead screw can amplify the motor driving force for it divides the driving distance in many motor's turns. More importantly, lead screw can significantly improve the precisions of position control. By using motor driving lead screw, we can obtain the position of Y in another way,

$$y_0 = ph \cdot m \quad (7)$$

Where, m is the number of the motor turns, Ph is screw lead.

If obtain the accurate datas of the position of the target position of the arm, the number of the MSL units, the position of initial Y direction, the length of the bar, and the screw lead, we can easily solve the actual motor turns we input,

$$\Delta m = (y_0 - y_1) / ph = ((ph \cdot m - x \cdot \tan(\arccos(x/n \cdot l)) / n) / ph) \quad (8)$$

Where, Δm is the number of the actual motor turns. When $\Delta m > 0$, then the motor rotates forward. When $\Delta m < 0$, then the motor reverses. Otherwise, the motor keeps stopping.

Summary

The novel robotics arm not only possesses satisfactory mechanical properties and simple method of position control but also perform lager range of motion than conventional robotics arm. The MSLs arm can be used as modular component to construct the systems in various applications especially in tether play-out and retrieval system and steep terrain adherence for vertical and horizontal mobility.

Acknowledgements

This work is supported by the Guangzhou major project funding: The research and development of new industrial robotics arms based on high-manufacturing industries (2014J4500029).

References

- [1]. John J. Craig, Introduction to Robotics, Mechanics & Control, Addison-Wesley Publishing Company.
- [2]. Vu, K. K., Liew, J. Y. R., Anandasivam, K. Deployable Tension-Strut Structures: from Concept to implementation [J]. Journal of Constructional Steel Research, 2006. 62: 195-209.
- [3]. C. Gantes, J., Connor, J., Logcher, R.D., Combining Numerical Analysis and Engineering Judgment to Design Deployable Structures [R]. 1991, Massachusetts Institute of Technology: Cambridge,. P. 431-440.
- [4]. C. Gantes, An Improved Analytical Model for the Prediction of the Nonlinear Behavior of Flat and Curved Deployable Space Frames [R]. 1997, Department of Civil Engineering: Athens. P. 129-158.
- [5]. Dai, J.S., Li, D., Zhang, Q., Jin, G. Mobility Analysis of a Complex Structured Ball Based on Mechanism Decomposition and Equivalent Screw System Analysis [J].