

Approach of Reliability Approximation with Extent of Error for a Resistor under Weibull Setup

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Analytical determination of reliability of a complex system is item dependent and setup dependent and a very difficult task. In this paper we propose reliability approximation based on reliability bounds for one such engineering item - a Resistor with independent components having the Weibull distribution. Earlier approach for reliability approximation was discretization. We provide a different approach for reliability approximation so that one not only gets a clear idea about the extent of error but also can adjust reliability in terms of distributional parameters. This reliability approximation having the Weibull distribution can be of practical use and importance as reliability approximation is developed in terms of distributional parameters.

Keywords: Stress-Strength Model, System Reliability, Weibull distribution, Reliability bound, Reliability approximation, Extent of error.

Notations

$S_x(X)$	= Survival function (sf) of a random variable X evaluated at the time point x.
$F_x(X)$	= Corresponding cumulative distribution (df) function.
$W(\lambda, \alpha)$	= Weibull distribution with scale parameter λ and shape parameter α .
$E(X)$	= Expectation on random variable X.
R	= System reliability.
$U(\lambda, \lambda_V, \lambda_{R_1}, \lambda_{R_2})$	= Reliability upper bound under the Weibull setup.
$L(\lambda, \lambda_V, \lambda_{R_1}, \lambda_{R_2})$	= Reliability lower bound under the Weibull setup.
R^*_{approx}	= Reliability approximation when $m > 1$, $n > 0$ and $\alpha > 2$.
R^{**}_{approx}	= Reliability approximation when $m < 1$, $n > 0$ and $\alpha > 2$.
R^{***}_{approx}	= Reliability approximation when $m < 1$, $n < 0$ and $\alpha > 2$.
Error*	= Extent of error when $m > 1$, $n > 0$, and $\alpha > 2$.
Error**	= Extent of error when $m < 1$, $n < 0$ and $\alpha > 2$.
Error***	= Extent of error when $m < 1$, $n > 0$ and $\alpha > 2$.

1. Introduction

In the context of reliability, stress indicates (Kapur and Lamberson [4]) any agency that tends to induce failure. On the other hand Strength indicates any agency resisting failure. Under the stress-strength model, reliability is defined as the probability that strength is greater than stress.

Knowing the distribution function of stress and strength, (Gertsbakh [3]) the reliability of the system i.e. the probability that the strength S is greater than the stress Y can be obtained using an integral equation.

Ordinary transformation techniques due to Parzen [5] can be used to determine the system reliability when stress and strength distribution are directly known. However such analytical approaches virtually fail when the stress variable is made up of multiple random factors.

2. Problem in determination

For many engineering items, the stress or strength variables are themselves functions of multiple stochastic factors and problem arises in determination of reliability. Now-a-days there are three independent lines of attack. First line of attack is due to Taylor's series expansion. Second line of attack follows from range approximation method which is given by Roy and Dasgupta [11]. In third approach, continuous setup is replaced by a closely approximated discrete setup given by Roy [8].

3. Earlier works

D'Errico and Zaino [1] have used Taguchi's [14] concept of experimental design and they presented discretization approach for approximating the behavior of complex system. Later English et al [2] extended the some approach by increasing the number of discrete point. They compared discrete approximation with simulated values. But their study was of course limited to normal setup. Xie and Lai [6] have studied approximation of system reliability using one step conditioning. Xue and Yang [15] have established a stress-strength inference reliability model with strength degradation under the assumptions that stress-strength are statistically independent. They have also presented simple formulas for estimating upper and lower

bounds for stress-strength reliability. The concept of discrete concentration of Roy [7] was used by Roy and Dasgupta [12] for presenting discretizing procedure. Roy [9 - 10] have examined in details discrete normal and discrete Rayleigh Distribution in this process. Roy and Dasgupta [13] have proposed evaluation of reliability of complex systems by means of discretizing approach under the Weibull setup.

But discrete approximation for any engineering item cannot adjust in terms of the parameter of the distribution. Reliability bounds on the other hand are functions of distributional parameters. Keeping these issues in mind, we have approximated reliability based on reliability bounds.

4. Reliability bounds

For the purpose of our proposed work, we have considered a well-known engineering item for approximating the reliability based on reliability bounds. The choice of our engineering item is power dissipated by a resistor.

A resistor is made up of two resistances R_1 and R_2 connected in parallel. The power dissipated from the resistor is described by the following functional form:

$$Y = V^2 \left(\frac{1}{R_1} + \frac{1}{R_2} \right),$$

where Y is the shear stress, V is the voltage across each resistor, and R_1

and R_2 are two resistances.

Let us evaluate the reliability approximation based on reliability bounds for a resistor having the Weibull distributions for R_1, R_2 and V.

5. Reliability bounds under the Weibull life distribution

Let us assume that component random variables R_1, R_2 and V are independent having the following parametric set ups. $V \sim W(\lambda_V, \alpha), R_1 \sim W(\lambda_{R_1}, \alpha)$, and $R_2 \sim W(\lambda_{R_2}, \alpha)$. Let the built-in-strength S be such that S follows yet another $W(\lambda, \alpha)$. Under these assumption, we try to determine the bounds on system reliability R. For this, we consider the following lemmas.

Lemma 1: Let X be nonnegative function of a r.v. X, then for every t, $P(X \geq t) \leq \frac{E(X)}{t}$

Lemma 2: Let X be nonnegative function of a r.v. X, then for every t, $P(X \leq t) \geq 1 - \frac{E(X)}{t}$

Theorem 1: Upper bound $U(\lambda, \lambda_V, \lambda_{R_1}, \lambda_{R_2})$, for the system reliability R, for a Resistor having the Weibull distribution is given by

$$U(\lambda, \lambda_V, \lambda_{R_1}, \lambda_{R_2}) = \text{Min} \left[\left(\frac{\lambda_V}{\lambda} \right)^{\frac{1}{\alpha}} \frac{\Gamma(\frac{1}{\alpha} + 1) \Gamma(1 - \frac{2}{\alpha}) \{ \Gamma(\frac{1}{\alpha} + 1) \}^2}{2(\lambda_{R_1} \lambda_{R_2})^{\frac{1}{2\alpha}}}, 1 \right], \text{ for } \alpha > 2.$$

Proof: From the definition of reliability

$$\begin{aligned} R &= P(S \geq Y) \\ &= P\left(S \geq V^2 \left(\frac{1}{R_1} + \frac{1}{R_2} \right)\right) \end{aligned}$$

$$\begin{aligned}
 &= P(S \geq L), \text{ where } L = V^2 \left(\frac{1}{R_1} + \frac{1}{R_2} \right) \\
 &\leq E\left(\frac{E(S)}{L}\right), \text{ applying lemma 1.} \\
 &= E(S)E\left(\frac{1}{L}\right) \\
 &= E(S)E\left(\frac{1}{V^2 \left(\frac{1}{R_1} + \frac{1}{R_2} \right)}\right) \\
 &= E(S)E\left(\frac{1}{V^2}\right)E\left(\frac{1}{\frac{1}{R_1} + \frac{1}{R_2}}\right) \tag{1}
 \end{aligned}$$

Now using the relation between G.M. and H.M., (1) reduce to

$$R \leq E(S)E\left(\frac{1}{V^2}\right)E\left(\frac{1}{2}\sqrt{R_1}\sqrt{R_2}\right) \tag{2}$$

$$= \frac{E(S)E\left(\frac{1}{V^2}\right)E(\sqrt{R_1})E(\sqrt{R_2})}{2} \tag{3}$$

$$= \left(\frac{\lambda_V^2}{\lambda}\right)^{\frac{1}{\alpha}} \frac{\Gamma\left(\frac{1}{\alpha} + 1\right)\Gamma\left(1 - \frac{2}{\alpha}\right)\left\{\Gamma\left(\frac{1}{2\alpha} + 1\right)\right\}^2}{2(\lambda_{R_1}\lambda_{R_2})^{\frac{1}{2\alpha}}} = m, \text{ say,} \tag{4}$$

Therefore, under the Weibull distribution, upper bound for the system reliability R, for a Resistor is

$$U(\lambda, \lambda_V, \lambda_{R_1}, \lambda_{R_2}) = \left(\frac{\lambda_V^2}{\lambda}\right)^{\frac{1}{\alpha}} \frac{\Gamma\left(\frac{1}{\alpha} + 1\right)\Gamma\left(1 - \frac{2}{\alpha}\right)\left\{\Gamma\left(\frac{1}{2\alpha} + 1\right)\right\}^2}{2(\lambda_{R_1}\lambda_{R_2})^{\frac{1}{2\alpha}}}, \text{ for } \alpha > 2.$$

If upper bound crosses 1 then it should be truncated at 1. Hence

$$U(\lambda, \lambda_V, \lambda_{R_1}, \lambda_{R_2}) = \text{Min}\left[\left(\frac{\lambda_V^2}{\lambda}\right)^{\frac{1}{\alpha}} \frac{\Gamma\left(\frac{1}{\alpha} + 1\right)\Gamma\left(1 - \frac{2}{\alpha}\right)\left\{\Gamma\left(\frac{1}{2\alpha} + 1\right)\right\}^2}{2(\lambda_{R_1}\lambda_{R_2})^{\frac{1}{2\alpha}}}, 1\right], \text{ for } \alpha > 2.$$

It completes the proof of theorem 1.

Theorem 2: Lower bound $L(\lambda, \lambda_V, \lambda_{R_1}, \lambda_{R_2})$, for the system reliability R, for a Resistor having the Weibull distribution is given by

$$L(\lambda, \lambda_V, \lambda_{R_1}, \lambda_{R_2}) = \text{Max}\left[0, 1 - \sqrt{2}\Gamma\left(1 - \frac{1}{2\alpha}\right)\left(\frac{\sqrt{\lambda}}{\lambda_V}\right)^{\frac{1}{\alpha}}(\lambda_{R_1} + \lambda_{R_2})^{\frac{1}{2\alpha}}\right], \text{ for } \alpha > \frac{1}{2}.$$

Proof: From the definition of reliability

$$\begin{aligned}
 R &= P(S \geq Y) \\
 &= P(S \geq V^2(\frac{1}{R_1} + \frac{1}{R_2})) \\
 &= P(V \leq \sqrt{\frac{R_2 S R_1}{R_2 + R_1}}) \\
 &= P(V \leq L'), \text{ where } L' = \sqrt{\frac{R_2 S R_1}{R_2 + R_1}} \\
 &\geq 1 - E(\frac{E(V)}{L'}), \text{ applying lemma2.} \\
 &= 1 - E(V)E(\frac{1}{L'}) \\
 &= 1 - E(V)E(\frac{1}{\sqrt{S}})E(\sqrt{\frac{R_1 + R_2}{R_1 R_2}}) \tag{5}
 \end{aligned}$$

$$R \geq 1 - E(V)E(\frac{1}{\sqrt{S}}) \frac{\sqrt{2}}{E(\sqrt{Min(R_1 R_2)})} \tag{6}$$

$$= 1 - \sqrt{2}\Gamma(1 - \frac{1}{2\alpha})(\frac{\sqrt{\lambda}}{\lambda_V})^{\frac{1}{\alpha}}(\lambda_{R_1} + \lambda_{R_2})^{\frac{1}{2\alpha}} = n, \text{ say,} \tag{7}$$

Therefore, under the Weibull distribution, lower bound for the system reliability R, for a Resistor is

$$L(\lambda, \lambda_V, \lambda_{R_1}, \lambda_{R_2}) = Max[0, 1 - \sqrt{2}\Gamma(1 - \frac{1}{2\alpha})(\frac{\sqrt{\lambda}}{\lambda_V})^{\frac{1}{\alpha}}(\lambda_{R_1} + \lambda_{R_2})^{\frac{1}{2\alpha}}], \text{ for } \alpha > \frac{1}{2}.$$

Because the lower bound cannot fall below zero. It completes the proof of theorem2.

6. Reliability approximation and error term

We propose the mean of the upper and lower bound as the approximate value of the system reliability and half of the absolute deviation between the two bounds as the extent of error. Let us discuss the three cases to derive reliability approximation and error terms. This reliability approximation and corresponding error terms can be expressed in terms of distributional parameters.

Case1: Reliability approximation and error term when m>1, n>0 and α > 2

Using the theorem1 and theorem2, we propose to approximate the system reliability as

$$\begin{aligned}
 R^*_{approx} &= \frac{[Min(m,1) + Max(0, n)]}{2} \\
 &= 1 - \{\Gamma(1 - \frac{1}{2\alpha})(\frac{\sqrt{\lambda}}{\lambda_V})^{\frac{1}{\alpha}}(\lambda_{R_1} + \lambda_{R_2})^{\frac{1}{2\alpha}}\} / \sqrt{2} \tag{8}
 \end{aligned}$$

This is a function of distributional parameters. Therefore, we can adjust it in respect of distributional parameters.

Extent of error is given by

$$\begin{aligned} \text{Error}^* &\leq \frac{[\text{Min}(m,1) - \text{Max}(0,n)]}{2} \\ &= \left\{ \Gamma\left(1 - \frac{1}{2\alpha}\right) \left(\frac{\sqrt{\lambda}}{\lambda_V}\right)^{\frac{1}{\alpha}} (\lambda_{R_1} + \lambda_{R_2})^{\frac{1}{2\alpha}} \right\} / \sqrt{2} \end{aligned} \tag{9}$$

Case2: Reliability approximation and error term when $m < 1, n > 0$ and $\alpha > 2$

Under this assumption, using theorem1 and theorem2, we suggest to approximate the system reliability as

$$\begin{aligned} R^{**}_{approx} &= \frac{[\text{Min}(m,1) + \text{Max}(0,n)]}{2} \\ &= \left[\left(\frac{\lambda_V^2}{\lambda}\right)^{\frac{1}{\alpha}} \frac{\Gamma\left(\frac{1}{\alpha} + 1\right) \Gamma\left(1 - \frac{2}{\alpha}\right) \left\{ \Gamma\left(\frac{1}{2\alpha} + 1\right) \right\}^2}{2(\lambda_{R_1} \lambda_{R_2})^{\frac{1}{2\alpha}}} \right. \\ &\quad \left. + 1 - \sqrt{2} \Gamma\left(1 - \frac{1}{2\alpha}\right) \left(\frac{\sqrt{\lambda}}{\lambda_V}\right)^{\frac{1}{\alpha}} (\lambda_{R_1} + \lambda_{R_2})^{\frac{1}{2\alpha}} \right] / 2 \end{aligned} \tag{10}$$

Extent of error is given by

$$\begin{aligned} \text{Error}^{**} &\leq \frac{[\text{Min}(m,1) - \text{Max}(0,n)]}{2} \\ &= \left[\left(\frac{\lambda_V^2}{\lambda}\right)^{\frac{1}{\alpha}} \frac{\Gamma\left(\frac{1}{\alpha} + 1\right) \Gamma\left(1 - \frac{2}{\alpha}\right) \left\{ \Gamma\left(\frac{1}{2\alpha} + 1\right) \right\}^2}{2(\lambda_{R_1} \lambda_{R_2})^{\frac{1}{2\alpha}}} \right. \\ &\quad \left. - 1 + \sqrt{2} \Gamma\left(1 - \frac{1}{2\alpha}\right) \left(\frac{\sqrt{\lambda}}{\lambda_V}\right)^{\frac{1}{\alpha}} (\lambda_{R_1} + \lambda_{R_2})^{\frac{1}{2\alpha}} \right] / 2 \end{aligned} \tag{11}$$

Case3: Reliability approximation and error term when $m < 1, n < 0$ and $\alpha > 2$

Under this assumption, using theorem1 and theorem2, we propose to approximate the system reliability as

$$\begin{aligned} R^{***}_{approx} &= \frac{[\text{Min}(m,1) + \text{Max}(0,n)]}{2} \\ &= \left(\frac{\lambda_V^2}{\lambda}\right)^{\frac{1}{\alpha}} \frac{\Gamma\left(\frac{1}{\alpha} + 1\right) \Gamma\left(1 - \frac{2}{\alpha}\right) \left\{ \Gamma\left(\frac{1}{2\alpha} + 1\right) \right\}^2}{4(\lambda_{R_1} \lambda_{R_2})^{\frac{1}{2\alpha}}} \end{aligned} \tag{12}$$

Extent of error can be given as

$$\begin{aligned} \text{Error}^{***} &\leq \frac{[\text{Min}(m,1) - \text{Max}(0,n)]}{2} \\ &= \left(\frac{\lambda_V^2}{\lambda}\right)^{\frac{1}{\alpha}} \frac{\Gamma\left(\frac{1}{\alpha} + 1\right) \Gamma\left(1 - \frac{2}{\alpha}\right) \left\{ \Gamma\left(\frac{1}{2\alpha} + 1\right) \right\}^2}{4(\lambda_{R_1} \lambda_{R_2})^{\frac{1}{2\alpha}}} \end{aligned} \tag{13}$$

7. Numerical study

By varying the mean strength parameter λ , we make a numerical study of reliability approximation along with the extent of error. The specific choices of distributional parameters are $\lambda_V = 25$, $\lambda_{R_1} = 4$, $\lambda_{R_2} = 5$. The corresponding reliability approximations and error terms have been provided in Table 1. It may be observed that error term sharply decreases as reliability increases.

8. An application of the proposed work

Unlike simulation method or discrete approximation method, design parameters can be adjusted under this method. Hence it can be of practical use during the early stages of product design. As reliability bounds are function of design parameters, are very important for product planning when neither the discrete approximation nor the actual values are available. There are cases where discrete approximations are extremely weak. For example, under the exponential setup, where lack of memory property holds, the discretization approach does not offer close approximate values. In that situation, one may depend on reliability bounds.

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Appendix

Table 1: Study of reliability approximation and error terms under the Weibull distribution for shape parameter $\alpha = 3$.

Strength parameter λ	Reliability approximation	Extent of error
.0009	.877654	.122346
.0008	.880032	.119968
.0007	.882672	.117328
.0006	.885648	.114352
.0005	.889071	.110929
.0004	.893119	.106881
.0003	.898119	.101877
.00025	.901173	.098828
.00020	.904780	.095220
.00015	.909238	.090763
.00012	.912551	.087449
.00010	.915168	.084832
.00005	.924423	.075577
.00004	.9272183	.072818
.00003	.930591	.069409
.00002	.935126	.064874
.00001	.942204	.057796
.000007	.945539	.054460
.000003	.952712	.047288
.0000015	.957871	.042129
.0000007	.962896	.037104
.0000003	.967783	.032217
.0000001	.973173	.026827
.00000002	.979484	.020516
.00000001	.981722	.018278
.000000001	.987548	.012453
.0000000001	.991516	.008484
.000000000001	.996062	.003938